



**User's Guide**

**Contamination Transport Simulation Program (CTSP)**

**Version 1.9.9**

**May 26th, 2025**



Particle In Cell Consulting LLC

[ctsp-sim.com](http://ctsp-sim.com)

[info@particleincell.com](mailto:info@particleincell.com)

## Contents

I. Introduction.....	3
I.a) License.....	3
I.b) Getting Started.....	3
I.c) A “Hello World” Example.....	4
I.d) Data Visualization.....	5
I.e) Parallel Processing.....	7
I.f) Online GUI.....	8
I.g) Future Work and Revision History.....	9
II. Operations Reference.....	11
II.a) General.....	12
II.b) Simulation Control.....	14
II.c) Ambient Environment.....	16
II.d) Materials.....	18
II.e) Interactions.....	20
II.f) Surface Geometry.....	21
II.g) Sources.....	25
II.h) Surface Output.....	31
II.i) Particle Output.....	33
II.j) Volume Mesh.....	35
III. Governing Equations.....	37
III.a) Molecular Contamination.....	37
III.b) Particulates.....	39
III.c) Particle Motion and Surface Impact.....	41
III.d) Subcycling.....	43
IV. Examples.....	44
IV.a) Vacuum Bakeout.....	44
IV.b) Molecular Equilibrium.....	50
IV.c) Particulate Transport.....	53
IV.d) Additional Examples.....	60
.....	61
V. References.....	62

## I. Introduction

Contamination Transport Simulation Program (CTSP) is a computer program for simulating transport of molecular and particulate contaminants [1]. These contaminants include hydrocarbons that diffuse out of materials exposed to vacuum as well as dust particles shaken off by vibrational loads. The code supports two simulation approaches. First, utilizing principles from the Particle in Cell (PIC) [2] and Direct Simulation Monte Carlo (DSMC) [3] techniques used by the plasma and rarefied gas community, contaminants can be represented by simulation *macroparticles*, with each macroparticle corresponding to some (typically) large number of real molecules. This scaling assures that the correct mass transport is simulated regardless of the actual number of particles in the simulation. Particle positions and velocities are advanced through small simulation time steps. Velocities change according to specified spatially and time-varying gravitational, electrostatic, or aerodynamic drag forces. On surface impact, the particles bounce off based on surface physics models, or are adsorbed to the target element surface layer. The code concurrently simulates the entire contaminant population, giving it the ability to consider inter-particle interactions (collisions) that may be of importance during events such as chamber repressurization. The concurrent simulation also allows the user to visualize densities (and other macroscopic properties) of the contaminant plume. The model is described in more detail in Section III. In addition, as of version 1.5, it is also possible to use the particles to compute black-body view factors from selected source element groups. These view factors can then be used to simulate mass transport over an extended period of time during which surface properties such as temperature or coefficient of restitution vary. The latest code version can be found at [ctsp-sim.com](http://ctsp-sim.com)

### I.a) License

Please review **LICENSE.txt** included with the code. Your use of the code implies consent to the license agreement.

### I.b) Getting Started

CTSP is a command line code available for Microsoft Windows and Linux (Ubuntu and Red Hat) platforms. To use the code, navigate to the directory containing the simulation input file, **ctsp.in**. To run the program, launch the **ctsp** executable. For example, on Microsoft Windows:

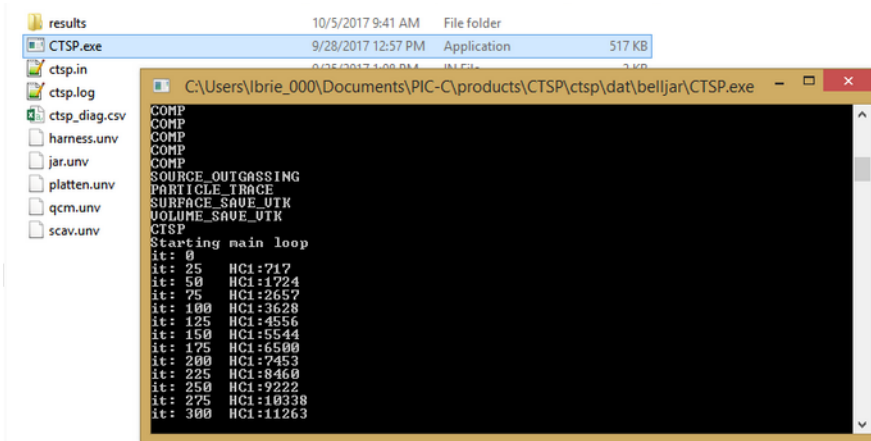


Figure 1. CTSP running on Microsoft Windows 8.1

In the Unix shell environment, we first navigate to the folder using **"cd"**. The code is launched using **"/.ctsp"** assuming the executable is placed in the same directory.

CTSP requires that a valid license file, typically called **ctsp.lic**, is found. The following locations are checked:

1. Path (including the file name) specified by **options{license\_file}** value.
2. Path (including the file name) specified by command line option **-l** (lowercase L)
3. "ctsp.lic" file in the current directory
4. "ctsp.lic" file in user's home directory. On Unix, this correspond to the \$HOME environmental variable, and on Windows this is the combination of \$HOMEDRIVE and \$HOMEPATH.

Simulation results are saved in a sub-folder called **"results/"**. This directory will be created automatically if it does not exist.

### I.c) A "Hello World" Example

Let's consider a simple case of computing molecular contamination due to outgassing on a generic satellite<sup>1</sup> as shown in Figure 2.

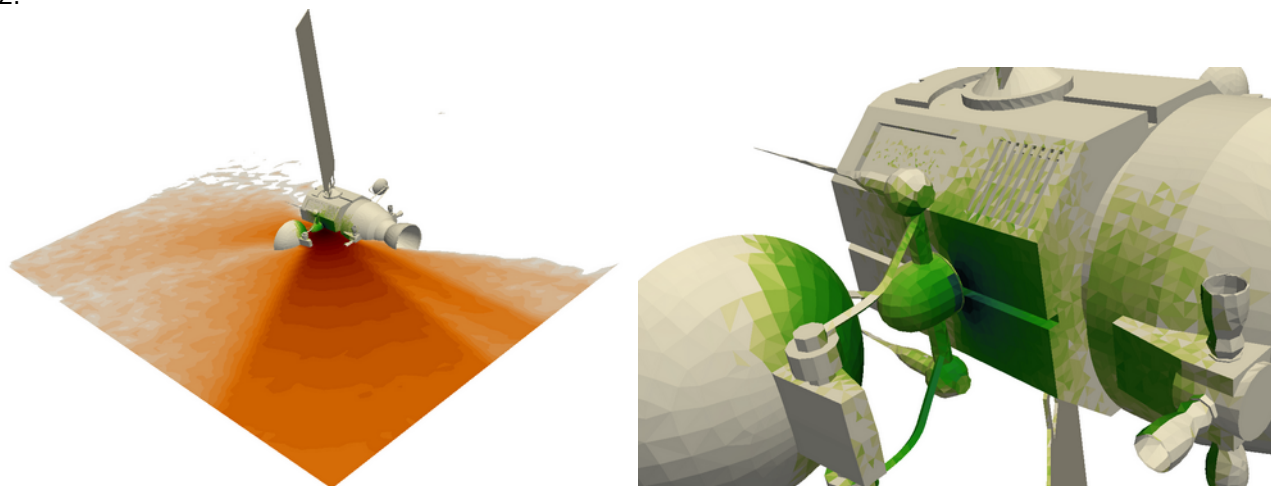


Figure 2. Contaminant plume and surface deposition on a generic satellite

Running this simulation consists of the following steps:

1. Loading the surface mesh(es). The satellite geometry is stored in a "satellite.unv" Universal file. The geometry could optionally be split into multiple files, with transformations such as translation, rotation, or scaling applied to each.
2. Specifying an optional Cartesian volume mesh. If present, the mesh is used to compute volumetric flow data such as the contaminant plume density which was used to produced the visualization in the first plot above. This mesh \*is not\* used during the particle push, except for bounds checking. Particles leaving the volume mesh are removed from the simulation.
3. Specifying material and material-interaction properties. The code does not contain a materials database and all solid and flying materials and their interactions need to be defined.
4. Specifying surface properties. This assignment is done on a "component" level, where components are groups of surface triangles and/or quads specified in the meshing program and stored in the mesh file. These groups typically correspond to physical objects such as radiators, solar panels, vents, and so on. We can assign material composition and time-dependent surface temperature.
5. Enabling material sources, such as outgassing. Outgassing is modeled by loading an initial concentration of molecules in the substrate and on the surface and specifying a desorption model. The code includes other source models specific to loading particulates or simulating prescribed flux vents.
6. Enabling output diagnostics, such as surface and volume plots, particle traces, and surface concentration histograms. The code supports the VTK (for Visit and Paraview) and Tecplot formats.
7. Running the simulation, and analyzing the results

An example **ctsp.in** input file is included below.

# "Hello World" example of modeling molecular contamination using particles

```
#simulation options
options{num_threads:1}
```

```
#load surface mesh, CAD model from https://grabcad.com/library/satellite-11
surface_load_unv{file_name:"satellite.unv"}
```

```
#define volume mesh for computing contaminant plume
volume_mesh{dx:0.02,dy:0.02,dz:0.02,expand:[0.5,0.5,0.5]}
```

```
#specify materials
```

<sup>1</sup>Pointwise, Inc. provided the mesh. CAD drawing from <https://grabcad.com/library/satellite-11>

```

solid_mat{name:blanketing, density: 2000}
solid_mat{name:sink, density: 2000}
molecular_mat{name:hc1, weight: 54, mpw: 1e10, Ea:12, r:2.776e-10, compute_fluid_properties:true}
molecular_mat{name:hc2, weight: 98, mpw: 1e9, Ea:10, r:4.0e-10, compute_fluid_properties:true}

#specify surface properties
surface_props{comps:././, mats:blanketing, temp:260, c_stick:1.0}
surface_props{comps:source, temp:1000}

#enable outgassing
load_molecules{comps:source, trapped_mass:1e-10, trapped_mats:hc1, surf_mats:hc2, surf_h:1e-10}
source_outgassing{model:"power"}

#alternative way to introduce molecules is by specifying surface sources
source_cosine{comps:source, mats: hc1, mass_flux:1e-3, v_drift:100}

#specify file output options
surface_save_vtk{file_name:surf, vars:[surf_height.hc1, surf_height.hc2, temperature],skip:100}
volume_save_vtk{file_name:field,vars:[nd.hc1, nd.hc2],skip:100}

#run simulation, perform screen/log file output every 5 time steps
run_sim{dt:1e-5,num_ts:1000, log_skip:5, fields_skip:100}

#save final results
volume_save_vtk{file_name:field,vars:[nd.hc1, nd.hc2]}
surface_save_vtk{file_name:surf, vars:[surf_height.hc1, surf_height.hc2, temperature]}

```

## I.d) Data Visualization

CTSP supports saving simulation results in VTK and Tecplot file formats. The Tecplot support is mainly retained for legacy and is quite limited. Therefore, it is recommended to use the VTK format. These files can be opened in Paraview ([www.paraview.org](http://www.paraview.org)) or VisIt ([visit.llnl.gov](http://visit.llnl.gov)), both of which are available for free. Below we demonstrate how to perform a typical visualization in Paraview. After the simulation finishes,

```

ts: 990      HC1:524592 HC2:738
ts: 995      HC1:525723 HC2:731
ts: 1000     HC1:526805 HC2:716
Writing results/surf_01000.vtp
Writing mesh results/field_01000.vti (structured)
Main loop ended on rank 0 of 1
Simulation of real 0.010000s took 1.907203 minutes.
Writing report to ctsp_report.txt
Processing VOLUME_SAVE_VTK
Writing mesh results/field.vti (structured)
Processing SURFACE_SAVE_VTK
Writing results/surf.vtp
Done!

```

folder called "results" will contain several files including "surf.vtp" and "field.vti". The former contains surface-based results, such as the height of the deposited contaminants. The latter file contains volumetric data such as the number density of the contaminant plume. Open these two files in Paraview. If not done so already, it is recommended to enable "Auto Apply" under Edit->Settings->General and change the background and text colors under Color Palette to white and black, respectively. You should obtain a view similar to what is shown below.

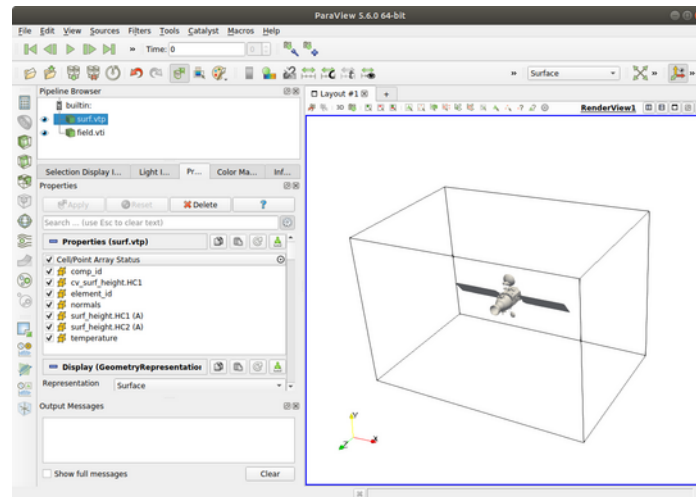


Figure 3. Initial view of results in Paraview

The Visualization Toolkit (VTK), which the Paraview is built on top of, uses the concept of a "visualization pipeline" to produce plots. The pipeline begins with the data, and is then transformed via multiple filters. The output of one filter can serve as an input to another. These outputs can be plotted in several ways, including "surface" and "surface with edges" (to show cell edges). Next, with "surf.vtp" selected in the Pipeline Browser, change "Coloring" on the "Properties" tab from "Solid Color" to "surf\_height.HC2". On "Color Map Editor" (enable under View menu if not visible), use the "folder with a heart" icon in the vertical toolbar to pick a different color scheme, such as "Black, Orange, White". Next click the "white/black circle" icon to invert the colormap to make white correspond to the low values and black to high values. Then use the "Rescale to Custom Range" button in this same vertical stack to set the range to  $1e-4$  to  $0.1$ . Next click the "colorbar with an e" icon to adjust legend properties. Click the "gear" icon next to the Search bar, and uncheck "Add Range Labels". This will make the number consistent as by default the colorbar range is printed using scientific notation. Also, on the Color Map Editor tab, enable "Use log scale when mapping data". Next interact with the geometry using the mouse. Holding down the right button while moving the mouse zooms. The middle button pans, while the left button rotates. You should obtain a view as shown in Figure 4.

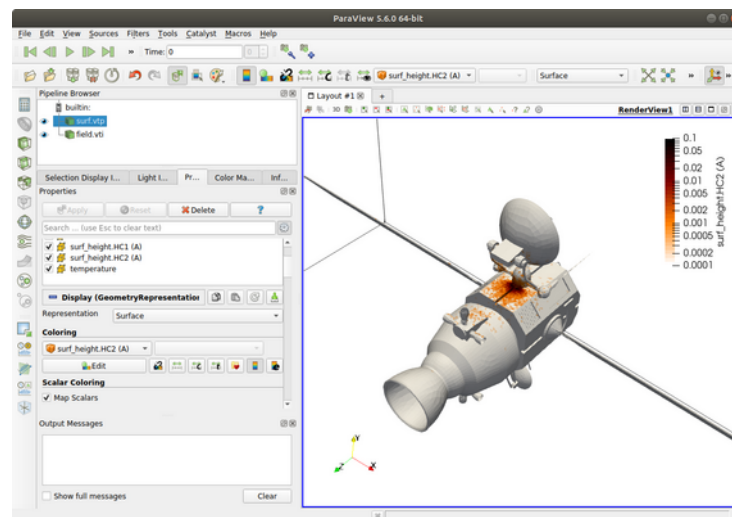


Figure 4. Visualization of surface data

Next, pressing "s" enables us to enter an interactive selection mode of cell data. Other selections can be enabled by clicking the small icons just above the blue border of the render view. Then, under "Selection Display Inspector" (enable under View menu), you can assign a specific variable for "Cell Labels". Here you can also change the color of the

selection border, and the font, color, and number format (using the C printf syntax) of the displayed number (%.2g means to show a floating point number with two significant digits).

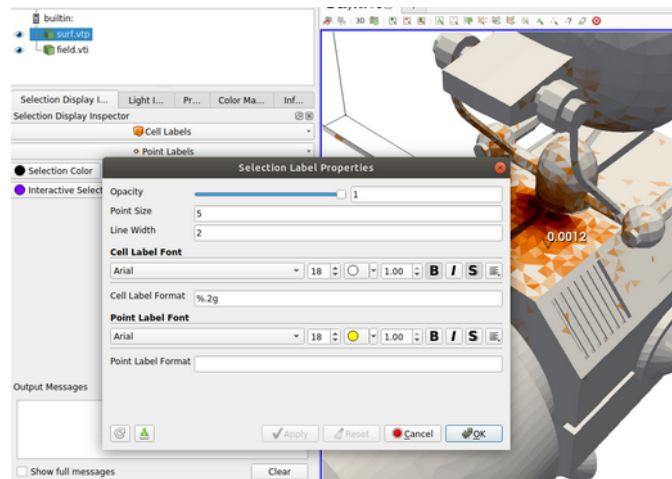


Figure 5. Use of selection inspector to visualize deposition on a surface element

Next, we select "field.vti" in the pipeline and use the "Slice" button to add a filter to plot data on a single 2D slice. Next selecting "field.vti" again, another slice can be added, with a different orientation. We can use the Color Map Editor to further change the data range, or to "enable opacity mapping for surfaces" to make data below the minimum color map value transparent. The "Mapping Data" window can be used to interactively set the opacity transfer function. We generate a view as shown below.

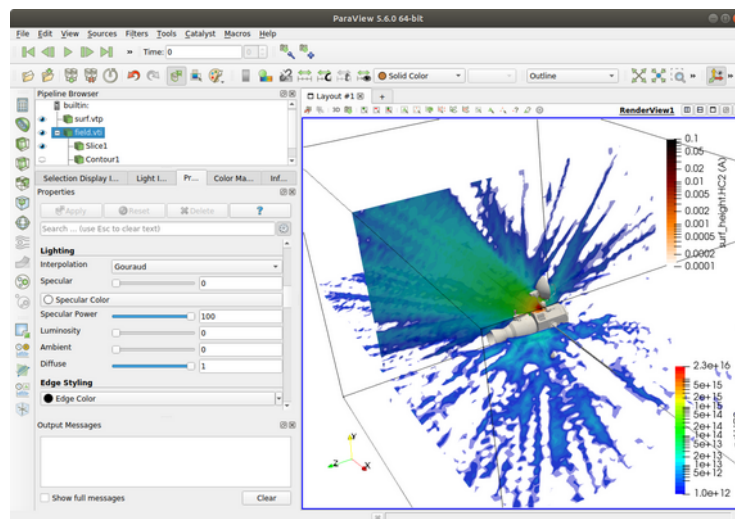


Figure 6. Use of selection inspector to visualize deposition on a surface element

## I.e) Simulation Report

As of version 1.9.8, CTSP also generates a simulation report written out to a file [input\_file\_name]\_report.txt, such as ctsp\_report.txt. This file summarizes in a tabular form information about the deposited mass or particulate loading on different zones. It also contains information about the run such as the total number of particles generated. Example is listed below:

##### CTSP SIMULATION REPORT #####

Version: 1.9.8  
Input File: ctsp.in  
Start Time: Wednesday, Nov 20, 2024 12:15:41  
Run Time: 0.324 minutes

Time Steps: 200

```

*****
Species      Generated      Escaped      Adsorbed      Remaining
-----
HC1           186173           0           86164         100009
HC2            0           0           0             0
TOTAL:        186173           0           86164         100009
*****

***** SOURCES *****
Source      mass_gen(kg)      mdot(kg/s)
-----
SOURCE_OUTGASSING_<>      1.26e-12      6.29e-10
SOURCE_COSINE_SOURCE_HC1  1.67e-10      8.35e-08
SOURCE_DESORPTION_SOURCE  0.00e+00      0.00e+00
*****

*****
Surface      Zone      MOLECULAR      DEPOSITION      THICKNESS (A)
-----
Id      T(K)      Total      HC1      HC2
-----
SURF         SOURCE      0      1000.0      1.15e+00      1.53e-01      1.00e+00
SURF         UNV_0003      1      260.0      1.12e-03      1.12e-03      0.00e+00
*****

*****
Surface      Zone      MOLECULAR      DEPOSITION      MASS (g)
-----
Id      T(K)      Total      HC1      HC2
-----
SURF         SOURCE      0      1000.0      6.34e-09      1.27e-09      5.07e-09
SURF         UNV_0003      1      260.0      7.72e-08      7.72e-08      0.00e+00
*****

*****
Surface      Zone      MOLECULAR      BULK MASS (g)
-----
Id      T(K)      Total      HC1      HC2
-----
SURF         SOURCE      0      1000.0      9.87e-08      9.87e-08      0.00e+00
SURF         UNV_0003      1      260.0      0.00e+00      0.00e+00      0.00e+00
*****

***** SURFACE DATA *****
Surface      Zone      Id      Momentum      NetEnergy      IncAngle      ChargeDen
-----
SURF         SOURCE      0      -1.53e-13      1.06e-11      101.54      0.00e+00
SURF         UNV_0003      1      6.39e-14      6.74e-12      1.32      0.00e+00
*****

***** TORQUE (Nm) *****
Surface      Centroid      MidPoint
-----
SURF         -1.28e-12      -3.32e-14      1.56e-13      -4.03e-11      4.19e-12      4.95e-10

```

## I.f) Parallel Processing

CTSP supports parallel processing via multithreading and MPI. CUDA support (for running on NVIDIA GPUs) is currently in development. CTSP implements two parallelization schemes. Bulk of the total computational effort involves advancing particle positions through time step  $\Delta t$ . This particle push is locally parallelized by assigning a subset of all particles to each CPU thread. The remaining parts of the code continue to run in serial. By default, if not run through MPI, the code utilizes the maximum number of concurrent threads supported by the CPU. On modern CPUs supporting hyperthreading, this will generally be twice the number of physical cores. Therefore, there may not be a noticeable speed up compared to using half this number. The number of threads to use is controlled via `options{num_threads:xxx}` command.

The code can also be run in parallel on multiple machines using “mpirun” (or mpiexec):

```
>mpirun -np 4 ./ctsp-ubuntu-mpi
```

Currently, only the Ubuntu and RedHat versions are shipped with MPI support enabled, but versions for other architectures can be provided on request. The MPI behavior differs from the multithreaded case described above. Instead of attempting to distribute the workload among processors, each MPI process runs the full simulation serially. The individual results are then ensemble-averaged for output. Running a parallel simulation on 10 cores is identical to running a single processor case with 10x as many numerical particles (the number of particles shown on the screen or in the log file will reflect the total particle count over the MPI domain). Example output from a parallel run is shown in Figure 7. The light yellow region in the figure on left corresponds to location with very little particle flux. The spotiness is due to numerical noise. Since each processor essentially runs a serial simulation with a different initial random number seed, we can use the local results to compute the coefficient of variation (normalized standard deviation) of the results on each surface element. This data is available by adding “cv\_” to the name of a surface or volume variable of interest. For example, “cv\_surf\_height” shows the variation in surface height, and thus allows us to determine the level of confidence in the contaminant build up prediction. A “cv” value of 0.1 indicates confidence within 0.1 standard deviations.



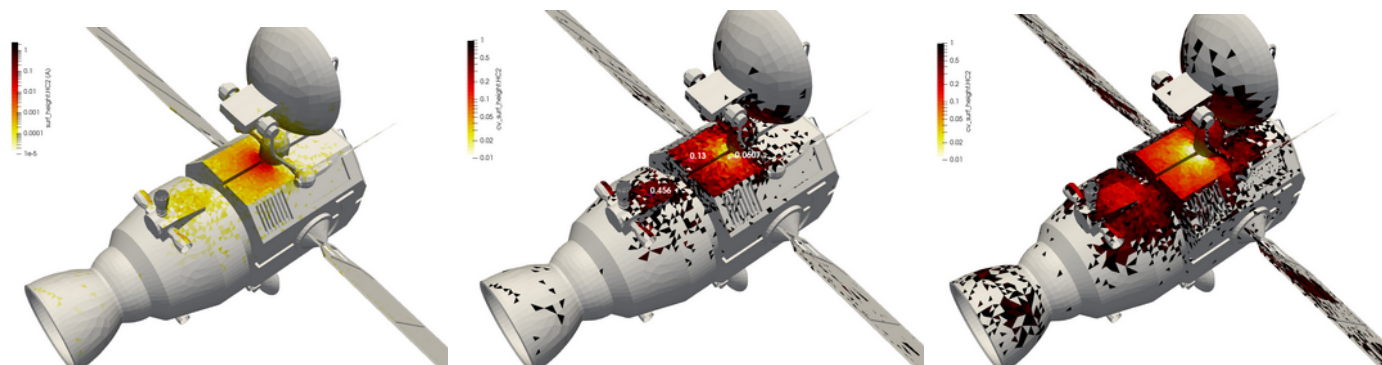


Figure 7. Plot of coefficient of variation from 6 and 48 CPU run

### I.g) Online GUI

While an actual GUI is still in development, the simulation input files can be generated with the help of a browser-based interface. The GUI has been tested with Firefox and Chrome. You can run the GUI either locally or from the code website <https://www.ctsp-sim.com/ctsp/>. Note that even when accessing the on-line version, the GUI runs locally on your machine and no information is transmitted to our server. The online GUI is currently updated only up to version 1.5 and thus should be used only to build initial input files which are to be modified later in a text editor.

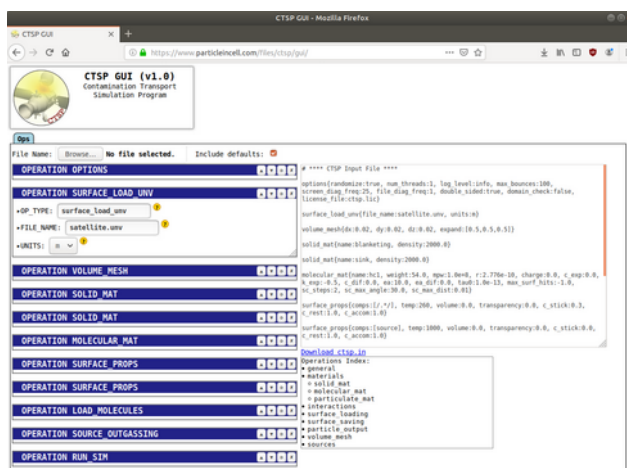


Figure 8. CTSP web-based GUI

The GUI consists of three sections: a list of operations showing all available options, a dynamic and automatically updated ctsp.in file, and an index of all available operations. Note that modifying the "OP\_TYPE" field also brings up a drop down list of matching operations, see Figure 4.

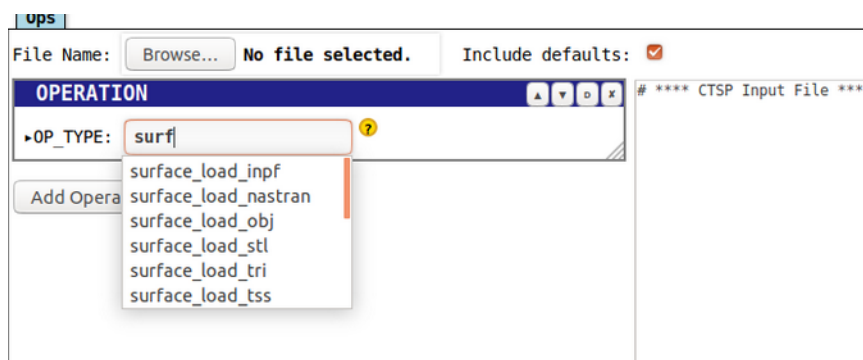


Figure 9. List of matching operations

To save the file, click the "download ctps.in" link or simply copy and paste from the output window.

## I.h) Known Bugs and Issue

Some known bugs include:

- Tecplot output functionality is likely broken
- Documentation examples section is out of date
- Online GUI is out of date

Current work includes the following:

- Addition of a Poisson solver
- Implementation of a GUI
- Additional work on surface dynamics
- Additional parallelization and port to GPU
- General code clean up and optimization
- Support for CAD-based geometries

Long term functionality

- Sputtering, atomic oxygen erosion, and orbital debris

## I.i) Revision History

- 1.9.9 Support for mesh refinement. Use of "compute\_fluid\_properties" to reduce memory in multispecies sims. Various bug fixes, including re-enabling parallel computation with CV calculation in both surface and volume results.
- 1.9.8 Addition of summary report generation on simulation exit.
- 1.9.7 Updates to surface dynamics model, as well as changes to surface adhesion calculation to eliminate dependence on time step.
- 1.9.6 Rabinovich surface adhesion model and surface dynamics
- 1.9.5 Addition of symmetry
- 1.9.4 Fix to parallelization crashes, addition of surface\_load\_FNF, work on surface dynamics. Arrhenius scaling for source\_cosine, addition of MLI temperature to TSS geometries
- 1.9.3 Improvements to surface dynamics, macroparticle count volume mesh output, surface\_generate command, changes to DSMC to support mixtures, save\_frames output flag
- 1.9.1 Preliminary support for surface dynamics (dynamic translation of surfaces). New license format.
- 1.9 Surface geometry now defined as a collection of surfaces. Each surface\_load\_XXX op can specify the name of the surface collection to load the geometry to. Subsequent operations, such as translation or animation, is specified using the named surface. Changes to Plume source to support components.
- 1.85 Addition of surface animation, new TSS shapes (ellipsoid/ogive), support for TSS submodels (grouping and SINDA loader), surface output of particle source elements and incident energy, addition of drag model of Loth, fixes to tapelift source
- 1.8 Rewrite of the surface checking algorithm to trace a single time step particle trajectory through the octree instead of checking against all surfaces in the step bounding box. This allows running simulations with much larger time steps than possible previously.
- 1.7 Addition of adsorption models based on vapor pressure curves, solution continuation across multiple TSS files, loading of temperatures from SINDA files
- 1.5 Major update introducing mat-mat interactions (no longer specified by surface\_props) allowing time-dependent coefficients and desorption models. New support for splitting the input into multiple files, include variables, add loops, integrate results, and save element-id averaged restart data to support simulating systems with time-varying surface models. SurfaceSaveVTK operation now takes a list of variables to output and supports outputting coefficient of variation from parallel runs. The octree used for storing data has been revamped, although optimization is ongoing. In addition, the TSS loader has been improved to handle assembly transformations, and surface temperature data loader has been added to load SINDA results. Initial work on computing black body viewfactors.
- 1.00 Major rewrite of the code base to reduce reliance on pointers, split of particulate sources into loading and generation, support for tape lift data, selection of particle integrator schemes, component-level surface deposition

histograms, external world force, periodic and symmetric flow data, web-based GUI, time step subcycling, better memory management

0.29 Fixes to particle surface handling, MPI, automatic creation of results directory, material density range

0.28.2 Addition of ISO-14644 source

0.28.1 Search for license file in user home directory

Please report any bugs or feature requests to [info@particleincell.com](mailto:info@particleincell.com).

## II. Operations Reference

CTSP simulations run according to commands specified in an input file. By default, the code searches for a file called **ctsp.in** in the current directory, but an alternative path can be specified as a command line argument. For instance:

```
> ./ctsp ../simulations/case2.in
```

The input file consists of multiple lines with the following format:

**#comment**

**operation{key1:value2, key2:value2, ...}**

Any line starting with a # is ignored. Each operation generally requires user inputs consisting of a “key” (the field name) and the corresponding values. The table below summarizes the value types.

type	description	example(s)
<b>bool</b>	Boolean value, can be one of <b>true</b> or <b>false</b>	key:true
<b>int</b>	Integer value	key:350
<b>float</b>	Double precision floating point value	key:1.4e-6
<b>float2</b>	Range of double precision values, or alternatively a single value	key:2000 or key:[2000, 4000]
<b>string</b>	A string value in optional quotation marks. May need to be a value from a list, or can be a regular expression between slashes	key:fairing key:./.*
<b>int3</b>	List of three integers bounded by square brackets	key:[3,4,5]
<b>i_list</b>	Arbitrarily long list of integers	key:[50,1000,1200,5000]
<b>float3</b>	List of three floating point values in square brackets	key:[0.2,0,1.2]
<b>f_list</b>	List of one or more floating point values in square brackets	key:[0,0.2,0,0,1.2,1.2]
<b>tuples</b>	Arbitrarily long list of float@float pairs	key:[300@0, 300@5, 100@6]
<b>s_list</b>	Arbitrarily long list of strings	key:[pressure,nd.hc1,t.hc1]
<b>s_comp</b>	Arbitrarily long list of float*string pairs with the float* part optional. Used to specify material composition. If the fraction part is omitted, the code assumes “1*”.	key:hc1 key:[0.6*hc1, 0.3*hc2, 0.1*n2]
<b>time</b>	Numerical value with optional d,h,m,s units included. Seconds are assumed if no units specified.	key:3d.2h

In additions, string variables can be substituted within dollar signs (\$...\$) and mathematical expressions can be included within a percent sign pair (%...%). The available operations are listed below. They are grouped by the operation type.

The remaining pages of this section provide information on different operations available in the code. Operations tagged with [DEMO] are available in Demo version.

## II.a) General

These operations provide support for “general” tasks such as setting program options or setting the global “world” environment.

II.a.1) SET_VARIABLE [DEMO]			
Adds a new variable that can be used in subsequent parts of the code within expressions wrapped by dollar (for direct substitution) or percent (to evaluate a simple mathematical relationship) signs. Variables are evaluated during the operation parsing.			
Key	Type	Default	Description
name	string		Variable name
value	string		Expression to evaluate. The code currently supports only basic arithmetic (+,-,*,/)
Example			
<pre>set_variable{name:T_substrate, value:273} set_variable{name:rads, value:rad_} # set rad_1, rad_2, rad_XYZ, etc... to 298K surface_props{comps:/\$rads\$.*/, temp:%T_substrate+25%}</pre>			

II.a.2) INCLUDE [DEMO]			
Inserts contents of the specified file at the current location. Can be used to split the simulation inputs into multiple physical files to reduce duplication.			
Key	Type	Default	Description
file_name	string		File to load
Example			
include{file_name:ctsp-master.in}			

II.a.3) OPTIONS [DEMO]			
Specifies various options. This op is processed first regardless of where it is located in the input file.			
Key	Type	Default	Description
randomize	bool	true	Will randomize the random number generator if true. Set to false to replicate the same simulation.
num_threads	int	np-1	Maximum number of threads to use for multithreading. By default set to CPU “number of cores” minus 1.
log_level	string	info	Specifies level of screen and file output. In order of decreasing output, one of [LOW, MEMORY, DEBUG, INFO, WARN, ERROR].
max_bounces	int	100	Maximum number of times a particle can hit a surface in a single time step before being flagged as “stuck”
double_sided	bool	true	Specifies whether surface contains double sided elements. If set to false, particles always reflect in the surface normal direction. If true, particles will reflect in anti-normal direction if hitting the back side. This however can lead to particle leaks so this should be set to false unless thin plate elements are actually present.
delete_back_side	bool	false	Deletes particles hitting a surface on the anti-normal side
domain_check	bool	false	Prints a warning message if particle leaves volume mesh. Useful for checking for particle leaks in a closed domain.
license_file	string	ctsp.lic	Path to the license file. Needs to be enclosed in quotes if “.” is present (in other words, if full path is specified on Windows)
surf_octree_maxdepth	int	5	Maximum number of surface octree subdivisions
surf_octree_test	bool	false	Run additional octree tests
temperature_update_s_kip	int	50	Number of time steps between surface temperature updates
save_surf_octree	bool	false	Outputs octree in VTU and .txt format
Example			
options{randomize:false,num_threads:2,log_level:info,license_file:"ctsp.lic"}			

II.a.4) RESTART_SAVE			
Saves data to a restart file.			

Key	Type	Default	Description
file_name	string	restart	Prefix for the restart file. ".bin" extension is added automatically, and in parallel runs, the rank is appended to the file name
skip	int	-1	Frequency of restart saves. If non-positive, the restart file is written out right away.
save_particles	bool	true	Controls whether particles should be saved
group_elements	bool	false	If true, surface deposition and bulk composition will be averaged over all elements with the same element id. This is currently only applicable to TSS geometries since other surface models do not support the same id to be shared among multiple elements
<b>Example</b>			
restart_save{skip:1000}			

II.a.5) RESTART_LOAD			
Loads restart data			
Key	Type	Default	Description
file_name	string	restart	Prefix of the restart file name to load
load_particles	bool	true	Skips loading particles if set to false
<b>Example</b>			
restart_load{file_name:restart2}			

## II.b) Simulation Control

These operations provide support for running the simulation. The simulation can be executed using either the "run\_sim", which starts simulating particles, or by using "compute\_viewfactors" to generate black body viewfactors which will then be used in a matrix-based gray body calculation (this functionality is still in development).

II.b.1) BLOCK_BEGIN / BLOCK_END [DEMO]			
Defines a repeatable block of commands. The block repeats for the given number of iterations as long as the condition evaluates to a non-zero value. Multiple blocks can be nested.			
Key	Type	Default	Description
repeat	int	1	Number of times the block should repeat
condition	string	1	Numerical expression to evaluate
Example			
<pre>#approximate outgassing over a 60 minute interval using 6 steps block_begin{repeat:6, condition: \$simulate_outgassing\$} run_sim{dt:1e-3, num_ts:1000} scale_outgassing{mats:*,factor: 600} world{add time:10m} block_end{}</pre>			

II.b.2) RUN_SIM [DEMO]			
Starts the main loop for a particle based simulation.			
Key	Type	Default	Description
dt	float		Simulation time step
num_ts	int		Number of time steps
ts_steady_state	int	0	Time step at which gas bulk property computation starts
fields_skip	int	10	Number of time steps between computation of volume data
log_skip	int	5	Number of time steps between screen and log file output. Generating this output requires parallel sync in MPI runs and hence could lead to a possible performance penalty.
ts_clear_particles	int	-1	Specifies time step at which particles should be deleted for steady-state averaging
desorption	bool	true	Controls if a default surface desorption source should be included
dt_integrate	float	dt	Specifies total real time this simulation corresponds to, used to control sticking of RES_TIME molecules
Example			
<pre>run_sim{dt:5e-6, num_ts:10000, log_skip:10}</pre>			

II.b.3) SCALE_OUTGASSING			
Advances surface deposition through dt seconds. Can be used to simulate a long time period using a sequence of simulations at intermediary time intervals.			
Key	Type	Default	Description
mats	s_list	*	List of materials to apply the operation to
dt	float		Integrates solution forward over "dt" seconds. Assumes the simulation attained steady state.
Example			
<pre>#approximate outgassing over a 2 hours using 2 steps run_sim{num_ts:2000,dt:1e-5, ts_steady_state:1000} scale_outgassing{mats:water,dt:3600} run_sim{num_ts:2000,dt:1e-5, ts_steady_state:1000} scale_outgassing{mats:water,dt:3600}</pre>			

II.b.4) STOP [DEMO]			
Stops processing the input file. Useful for testing instead of commenting out follow on ops.			
Key	Type	Default	Description
Example			

```
stop{}
```

#### II.b.5) COMPUTE\_VIEWFACTORS

Uses a specified material type to compute black body viewfactors for all elements of a given zone. Specifically, a user specified number of particles is launched from each element using a cosine source. These particles are propagated until hitting a surface or leaving the domain. Particles stick on the first surface impact. Since the same algorithm is used to push particles as during a regular simulation, it is possible to include the effect of charge, drag, or even collisions. The computed viewfactor can be visualized using "vf.el\_id" surface variable. **(IN DEVELOPMENT)**

Key	Type	Default	Description
comps	s_list		List of component groups to apply the op to
mat	string		Material to use for the calculation
particle_count	int	1000	Number of particles (rays) to generate per element
max_steps	int	10000	Maximum number of time steps per element. The loop terminates early once all particles are lost.
dt	float	1e-3	Simulation time step. Vel_mag*dt should be no more than 10% of the simulation bounding box.
vel_mag	float	1	Injection velocity. Can be set arbitrarily for free molecular flow (except that dt needs to be scaled accordingly to prevent an inefficiently-large bounding box when checking for surface hits).
log_file_name	string	vf.log	Name of a file to which view factors are saved, or set to blank for no output.

#### Example

```
compute_viewfactors{comps:vent,mat:hcl,dt:1e-3}
```



## II.c) Ambient Environment

This section includes operations for setting the ambient environment.

II.c.1) EFIELD_LOAD_CSV			
Loads electric field components (in V/m) from a file. This operation can be used to simulate effect of the electric field on charged particulates or molecules. The code uses the inverse-distance weighing methods to interpolate field components, which can lead to out-of-sight points being considered near corners.			
Key	Type	Default	Description
file_name	string		File to load
map_pos	int3	[0,1,2]	Column indexes for position
map_ef	int3	[3,4,5]	Column indexes for electric field components
Example			
efield_load_csv{file_name:efn.csv}			

II.c.2) FLOW_LOAD_CSV			
Loads flow data from a CSV file containing a point cloud of positions (in meters), velocities (m/s), and densities (kg/m <sup>3</sup> /s). Instead of density, pressures (Pa) and temperature (K) can be included. Multiple files can be loaded to correspond to different simulation times with linear interpolation used for intermediate values. The code uses the inverse-distance weighing methods to interpolate velocities, which can lead to out-of-sight points being considered near corners.			
Key	Type	Default	Description
file_name	string		File to load
map_pos	int3		Column indexes for positions
map_vel	int3		Column indexes for velocities
map_rho	int	-1	Column index for density. Either density or pressure with temperature need be listed, if given. If not included, the code uses the density data per <b>world</b> .
map_pressure	int	-1	Column index for pressure if density not listed
map_temperature	int	-1	Column index for temperature if density not listed
scale_rho	float2		Scales density per [0]*rho+[1]
scale_p	float2		Scales pressure per [0]*p+[1]
scale_T	float2		Scales temperature per [0]*T+[1]
scale_vel	float2		Scales velocity vectors per [0]*v+[1]
point_skip	int	1	Stride for loading points
mu	float	1.846e-5	Dynamic viscosity for Reynolds number calculation, default value is for dry air at 300K per <a href="http://www.engineeringtoolbox.com/dry-air-properties-d_973.html">www.engineeringtoolbox.com/dry-air-properties-d_973.html</a>
mode	string	NORMAL	One of [NORMAL, WEDGE_X/Y/Z, or SYMMETRY_X/Y/Z]. WEDGE_Z models axisymmetric wedge rotated about the z axis, while SYMMETRY options are used with data symmetric about a single axis.
dtheta	float	0	Mode WEDGE only: wedge width in degrees, zero for axisymmetry
x0	float3	0,0,0	Modes WEDGE and SYMMETRY only: Point on the axis for WEDGE or on the symmetric face for SYMMETRY
use_volume_grid	bool	false	If true, the flow data will be first interpolated to the volume grid, and particle data will be gathered from the grid. If false (default), loaded data, stored in an octree, is used directly.
dx_min	float	-1	Initial size of a interpolation bounding box. If -1, will be set to 1/1000 of the largest length of the flow data bounding box.
max_resizes	int	10	Maximum number the dx_min^3 box is doubled in size when searching for points
shep_p	float	2	Interpolation coefficient for the Shepard's method, $w=d(x,x_0)^{(-p)}$ .
time	float	0	Time in seconds for this data set. Multiple data sets can be loaded with the code linearly interpolating velocity data at in-between times.
end_time	float	-1	End time, in seconds. Only applicable to the last file in series.
Example			
<pre>flow_load_csv{file_name:"purge_1e-4.csv",map_pos:[4,5,6],map_vel:[0,1,2], time:-1,time:0} flow_load_csv{file_name:"purge_1e-3.csv",map_pos:[4,5,6],map_vel:[0,1,2], time:-1,time:5}</pre>			

**II.c.3) WORLD [DEMO]**

Specifies the ambient environment. Multiple commands can be included to simulate transient events. Alternatively, a .csv file containing temporal data can be provided. The world command can also be used to set or advance the simulation time. This is useful for setting initial time to correspond to transient surface temperature data, or to advance the solution in conjunction with "scale\_outgassing" op.

Key	Type	Default	Description
time	time	0	Simulation time corresponding to this entry
gravity	float3	[0,0,0]	Vector form of gravitational acceleration vector in m <sup>2</sup> /s
uniform_flow	float3	[0,0,0]	Vector form of uniform flow velocity in m/s
E_field	float3	[0,0,0]	Vector form of uniform electric field in V/m
F_ext	float3	[0,0,0]	Generic external force in N
density	float	0	Ambient gas density in kg/m <sup>3</sup>
pressure	float	0	Ambient pressure in Pascal
temperature	float	0	Ambient temperature in K, used to compute gas density if density not specified
accel_vibe	float	0	Magnitude of random vibrational acceleration, used to detach particulates
sun_direction	float3	[0,0,0]	Vector corresponding to ambient light, used for estimating photo-deposition
file_name	string		Optional CSV file for specifying time-dependent environment
periodic	bool	false	If true, data in the above file is assumed to be periodic, with period (time[last]-time[first]).
map_time	int		CSV file column index for time in seconds. Linear interpolation used for in-between data.
map_gravity	int3	[-1,-1,-1]	Column indexes for gravity vector, -1 indicates data not present
map_flow	int3	[-1,-1,-1]	Column indexes for flow velocities
map_ef	int3	[-1,-1,-1]	Column indexes for electric field components
map_fext	int3	[-1,-1,-1]	Column indexes for external force
map_density	int	-1	Column index for density
map_pressure	int	-1	Column index for pressure
map_temperature	int	-1	Column index for temperature
map_accel_vibe	int	-1	Column index for magnitude of random vibrational acceleration

**Time Setting**

set_time	time	-1	Sets current simulation time to the provided value if non-negative
add_time	time	0	Advances current simulation time by the given interval

**Example**

```
world{gravity:[-9.81,0,0],uniform_flow:[0.0,0,0], density:1.2}
world{file_name:accel.csv, map_time:0, map_gravity:[1,-1,-1],
  pressure:101325, temperature:300}
world{set_time:4m5s}
```

Example accel.csv file:

```
time, gx
0,-9.81
5,-12.6
70,-16.9
```

## II.d) Materials

These ops are used to define simulation materials.

II.d.1) SOLID_MAT [DEMO]			
Specifies a general non-flying material. Solid materials are currently used only to control diffusion in the Fang model.			
Key	Type	Default	Description
name	string		Material name
density	float	2000	Material density in kg/m <sup>3</sup> . Currently unused.
Example			
<code>solid_mat{name:al, density: 1000}</code>			

This table lists common parameters for all flying (molecular and particulate) materials:			
Key	Type	Default	Description
name	string		Material name
max_surf_hits	float	-1	If greater than zero, limits how many times a particle can hit a surface before becoming permanently stuck
sc_steps	int	2	Number of subdivisions used for subcycling check, <2 disables s/c (enabled by default for particulates)
sc_max_angle	float	30	Max angle (deg) between sub and non-subcycled velocity and position vectors
sc_max_dist	float	0.01	Max distance (m) between final position with and without s/c
compute_fluid_properties	bool	false	Determines whether material-specific macroscopic properties such as nd.sp, T.sp, and so on will be available. Defaults to false to avoid excessive memory usage in multi-species simulations.
drag_model	string	WHITE	Specifies drag model, one of [WHITE, LANE, LOTH]
c_lift	float	0	Lift coefficient
Example			
<code>particulate_mat{name:flakes, density_range:[1000,3000]}</code>			

II.d.2) MOLECULAR_MAT			
Specifies a molecular material which simulates gas particles with negligible mass.			
Key	Type	Default	Description
weight	float		Atomic weight in AMUs (daltons)
r	float	1.55e-10	Molecular radius in m
charge	float	0	Material charge in elementary charge units
mpw	float		Macroparticle weight - ratio of real to simulation molecules. This parameter notionally controls the number of particles in the simulation. Typical values are around 1e15 and can be computed from: $contam\_plume\_number\_density * domain\_volume = mpw * N_{sim}$ where a good starting point for $N_{sim}$ is 10,000. However, the code currently supports automatic mpw.
mpw_min	float	mpw	Smallest macroparticle to generate and track
mp_density	float	0	Number of macroparticles to generate per m <sup>2</sup> . If specified, will override the "mpw" parameter.
gamma	float	1.4	Heat ratio for plume model
sc_steps	int	1	Subcycling steps
antoine_coeffs	f_list		Coefficients for the Antoine equation [A,B,C,scale], $P=scale*10^{(A-B/(C+T))}$
antoine_min_temp	float	1	Temperature floor for Antoine equation
dsmc_omega	float	0	Omega coefficient used for DSMC VHS
dsmc_d	float	0	Molecular diameter for DSMC VHS
Ea	float	10	Default activation energy in (kCal/mol)
Ea_vap	tuples	10	Activation energy for vaporization, can be specified as a constant or a set of Ea@T tuples
Ea_sub	tuples	10	Activation energy for sublimation
Ea_dif	tuples	10	Activation energy for diffusion

C_dif	tuples	1	Diffusion coefficient
C_pow	tuples	1	Scaling coefficient for the power law model
k_pow	tuples	-0.5	Time constant for power law model
tau0	tuples	1e-13	Scaling value for residence time (molecular residence time)
c_stick	tuples	-1	Stick coefficient, will be used if non-negative
c_stick_perm	tuples	0	Sticking coefficient for permanent adhesion (photopolymerization)
sun_view_only	bool	false	If true, c_stick_perm only used on sun facing elements
use_dt_integrate	bool	false	Controls if dt_integrate value specified in RUN_SIM should be used to computed sticking for RES_TIME desorption model
desorption_model	string	res_time	One of [RES_TIME, ANTOINE, MURPHY_KOOP, C_STICK, NONE]. Controls the molecular desorption model. ANTOINE and MURPHY_KOOP models use the partial pressure evaluated at the surface temperature to compute desorption "capacity" and molecules stick until capacity is depleted.
time_constant	float	60	Time in seconds used to compute desorbion for model C_STICK

**Example**

```
molecular_mat{name:hcl, weight: 94, mpw: 1e13, Ea:12, C_dif:1, r:1.55e-10, k:[-1@0,-1@5,-0.5@5.1]}
```

**II.d.3) PARTICULATE\_MAT [DEMO]**

Specifies a particulate material. These are much larger than molecules and are affected by drag and gravity.

Key	Type	Default	Description
density	float2	1000	Density range in kg/m <sup>3</sup>
charge_density	float2	0	Particulate surface charge density range in C/m <sup>3</sup>
min_bounce_speed	float	0.001	Minimum reflected speed (in m/s) that a particulate must have not to stick to a surface
mpw_min	float	0	Minimum macroparticle weight for generation
adhesion_model	string	C_STICK	Selects surface adhesion model, one of [C_STICK, RABINOVICH]
youngs_modulus	float	1e9	Young's modulus, used by the Rabinovich model to compute compression

**Example**

```
particulate_mat{name:flakes, density_range:[1000,3000]}
```

## II.e) Interactions

This section covers operations that specify how materials interact with each other.

II.e.1) DSMC			
Turns on DSMC collisions between flying materials.			
Key	Type	Default	Description
mats	s_list		List of flying materials interacting in this process. All materials must have the same macroparticle weight.
process	string	VHS	Collision process. Currently only VHS (Variable Hard Sphere) is supported.
sigma	string		Cross-section model, one of [CONST, POW, VHS]
sigma_coeffs	f_list		List of coefficients for the cross-section model, $\sigma_{const} = c_0$ , $\sigma_{pow} = c_0 v_r^{c_1}$ VHS model coefficient obtained from molecular_mat properties.
sigma_cr_max	float	1e-16	Initial value for the $(\sigma \cdot c_r)_{max}$ product
Example			
<pre>molecular_mat{name:n2, weight: 28, mpw: 1e10, dsmc_d:6.27e-10, dsmc_omega:0.74} dsmc_pair{mats:[n2,n2],sigma_cr_max:1e-16,sigma:VHS}</pre>			

## II.f) Surface Geometry

The following operations are used to import surfaces and to set surface component properties. Components are logical groups of surface triangles or quadrangles mapping physical regions of interest. Surface geometries are grouped into a collection of surface “actors”, which can be assigned dynamic transformation (although this is still in development). A single surface can consist of multiple geometries loaded from different files. The surface to associate with the geometry is specified using the “surface\_name” loader property.

### II.f.1) LOAD\_TEMPERATURE

Loads time-dependent surface temperature data. Currently supports binary files written out by Fortran in of the two following formats:

#### Format BIN1:

```
NN: unsigned long number of nodes
el_id[0], el_id[1], ... el_id[NN-1]: NN unsigned long element ids
frame_time: double, time in seconds
T[0], T[1], ... T[NN-1]: temperatures for nodes
<repeat frames until EOF>
```

#### Format BIN2: (supports submodel mapping using a map file)

##### map file:

```
1 modelA 1
2 modelA 2
3 modelB 1
```

##### bin file:

```
frame_time: double, time in seconds
T[0], T[1], ... T[NN-1]: temperatures for nodes
<repeat frames until EOF>
```

The loader also supports several ASCII .csv formats. These include:

#### Format CSV. This format requires specifying temperature for each element id.

```
time, element1, element2, ...
xx, xx, xx
element is either an element_id or submodel.element_id
```

Format CSV\_CLOUD: This format uses inverse distance weighing method to interpolate point cloud data to surface elements. Requires a file of times, another file of temperatures, and another file of positions.

##### time file:

```
time1
time2
```

##### temperatures file :

```
T1, T2, T3
```

##### positions files:

```
x1, y1, z1
x2, y2, z2
x3, y3, z3
```

Key	Type	Default	Description
file_name	string		File to load
dt	float	5*3600	Only frames with time difference greater than dt are stored to reduce memory
save	int_list		List of element ids to write to an output file for testing
units	string	K	Temperature units, one of [C,F,K]
surface_name	string	surf	Surface to apply these temperatures to
format	int	csv	Format specifier, one of [BIN1, BIN2, CSV, CSV_CLOUD]
map_file	string		Text map file for format BIN2
file_name_t	string		File of times for the CSV_CLOUD format
file_name_temps	string		File of temperature columns for each time for the CSV_CLOUD format
file_name_pos	string		File of node positions for CSV_CLOUD, number of rows must match number of columns in the temperature file

### Example

```
load_temperature{file_name:"temps\element_temps.csv",format:csv,dt:100}
```

#### II.f.2) SURFACE\_DYNAMICS

Specifies velocity and rotation for surfaces. **In development.**

Key	Type	Default	Description
surface_name	string		Surface to apply dynamics to
time	float	0	Time at which to apply this velocity
velocity	float3	[0,0,0]	Linear velocity in m/s
rotational_velocity	float3	[0,0,0]	Rotational velocity vector (axis * magnitude in deg/s), <b>not yet working</b>
centroid	float3	-	Surface centroid to be used for torque calculation
skip	int	50	Number of time steps between updates

##### Example

```
surface_dynamics{surface_name:astrol,time:0,velocity:[100,10,10]}
```

#### II.f.3) SURFACE\_CLEAR

Deletes the surface mesh

Key	Type	Default	Description

##### Example

```
surface_clear{}
```

#### II.f.4) SURFACE\_GENERATE

Creates analytical surface. For now, only surfaces mapping to volume mesh faces can be created.

Key	Type	Default	Description
type	string		Surface to generate, one of [XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX]
comp_name	string		Name to assign to the surface group

##### Example

```
surface_generate{type:ZMIN,comp_name:zmin}
```

#### II.f.5) SURFACE\_LOAD\_FNF

Loads a surface in the FEM Neutral Format

Key	Type	Default	Description
file_name	string		File to load
surface_name	string	surf	Surface for this geometry
units	string	m	Dimension units, one of M, DM, CM, MM, IN
comp_names	slist		Group names, any missing groups are named "FNF_xxxx"
group_by	string	surf	One of [SURF,MAT,PROP]

##### Example

```
surface_load_fnf{file_name:"ptc.fnf",group_by:mat,comp_names:["p11","p12","el"]}
```

#### II.f.6) SURFACE\_LOAD\_INPF

Loads a surface in the INPF format generated by NX thermal solver

Key	Type	Default	Description
file_name	string		File to load
surface_name	string	surf	Surface for this geometry

##### Example

```
surface_load_INPF{file_name:INPF}
```

#### II.f.7) SURFACE\_LOAD\_NASTRAN

Loads a surface mesh in NX Nastran format. Component names obtained from "\$\* NX mesh:comp" lines.

Key	Type	Default	Description
-----	------	---------	-------------

file_name	string		File to load
surface_name	string	surf	Surface for this geometry
units	string	m	Dimension units, one of M,DM, CM, MM, IN
comp_name	string	default	Default component name
<b>Example</b>			
surface_load_nastran{file_name:"container.dat", surface_name:surf_container}			

**II.f.8) SURFACE\_LOAD\_OBJ**

Loads a surface mesh in the OBJ format. This format can be used to export directly from CAD programs without needing to mesh the geometry first. Component names are obtained from "g" or "o" tags.

Key	Type	Default	Description
file_name	string		File to load
surface_name	string	surf	Surface name for this geometry
units	string	m	Dimension units, one of M,CM, MM, IN
<b>Example</b>			
surface_load_obj{file_name:"../part.obj",units:mm}			

**II.f.9) SURFACE\_LOAD\_STL [DEMO]**

Loads a surface mesh in the STL ASCII format. This format is sometimes used to export directly from CAD. It does not support multiple components.

Key	Type	Default	Description
file_name	string		File to load
surface_name	string	surf	Surface to associate with this geometry file
units	string	m	Dimension units, one of M,CM, MM, IN
comp_name	string	default	Component name to assign to all elements in this file.
<b>Example</b>			
surface_load_stl{file_name:"part.stl",units:mm,comp_name:"part"}			

**II.f.10) SURFACE\_LOAD\_TRI**

Loads a surface mesh in the TRI format (<https://www.nasa.gov/publications/software>). Elements are grouped into numbered components, names for which are specified by "comp\_names" property.

Key	Type	Default	Description
file_name	string		File to load
surface_name	string	surf	Surface group to load into
units	string	m	Dimension units, one of M,CM, MM, IN
comp_names	s_list		List of component names to assign to each comp id
<b>Example</b>			
surface_load_tri{file_name:"next.tri", comp_names:[comp1,comp2,comp3,comp4]}			

**II.f.11) SURFACE\_LOAD\_TSS**

Reads a surface file in the thermal TSS file format. This format stores geometry as an assembly of primitive analytical shapes such as cylinders, rectangles, etc. Not all TSS objects are fully implemented. Version 1.5 comprises a major update to the TSS loader.

Key	Type	Default	Description
file_name	string		File to load
surface_name	string	surf	Surface group to load into
group_by	string		One of [ASSEMBLY, SHAPE, OPTICS, MATERIAL, ELEMENT, SUBMODEL], controls assignment of component names to TSS objects. These groupings correspond to assembly label, shape label, shape property from ["optics", "optics_xmin", "optics_gmin"], property from "material", or the actual element id
mapping	s_list		Name of a CSV file to use for mapping. The first column (column 0) corresponds to the TSS entity specified by grouping. The column given by the second parameter (1 by default) specifies the component name.
units	string	m	Sets default units, one of [m,cm,mm,in]



tolerance	float	1e-7	Optional tolerance for removing overlapping elements if tol>0
sun_view_file	string		A CSV file containing a list of element id to be flagged as viewing the sun, can be used to permanently stick contaminants
default_active	string	NONE	Active side to use if not specified, one of [UP,DOWN,IN,OUT,BOTH,NONE]
MLI_offset	int	-1	Node id offset used to indicate MLI temperatures. i.e. node_ids="1001,1002,1,2" with offset of 1000 implies that temperatures for 1 and 2 are used for outgassing, and temperatures for 1001 and 1002 are used for surface sticking and desorption

**Example**

```
surface_load_TSS{file_name:"model.tssgm", group_by:"element", mapping:["node2mat.csv", 1]} }

#node2mat.csv
node,mat
16603,aluminum
16604,aluminum
32306,SLI
```

**II.f.12) SURFACE\_LOAD\_UNV [DEMO]**

Loads a surface mesh in the Universal format, specifically as exported by Salome. Supports datasets 2411 (nodes), 2412 (elements), and 2467 (groups).

Key	Type	Default	Description
file_name	string		File to load
surface_name	string	surf	Surface to load into
units	string		Dimension units, one of M,CM, MM, IN

**Example**

```
surface_load_unv{file_name:"model/box.unv"}
```

**II.f.13) SURFACE\_LOAD\_VTK**

Loads a surface in a VTK .vtp or .vtu XML format. Currently only ASCII uncompressed data containing triangles or quads is supported. "Information" elements need to be manually trimmed out of the points data, if present (they are included when using Paraview Save Data feature).

Key	Type	Default	Description
file_name	s_list		File(s) to load
comp_names	s_list	default	Component names to assign to the mesh
comp_var	string		<del>Optional CellData variable to use for assigning component names. Variable needs to contain integer values 0,1,...,num_comp_names-1. If not specified, all elements are assigned to the first component.</del> <b>[IN DEVELOPMENT]</b>
units	string	M	Dimension units, one of M, CM, MM, IN

**Example**

```
surface_load_VTK{file_name:mesh.vtp,comp_names:[chamber,pump],comp_var:zone_id}
```

**II.f.14) SURFACE\_PROPS**

Specifies properties on one or more components (group of surface elements)

Key	Type	Default	Description
comps	s_list		Component these properties should be applied to. Can use RegEx wrapped in ./ (such as ./ to match all components).
mats	s_comp		String list of materials the component substrate is made of. This is currently not used but could be utilized in the future to model sputtering or other similar surface effects.
temp[erature]	tuples	300	Component temperature in K. Can specify a list of temp@time tuples such as [300@0, 100@50] for a linear ramp down from 300 to 100K over 50 seconds.
use_loaded_temp[erature]	bool	true	Controls whether temperature from LOAD_TEMPERATURE should be applied to this zone, if true (and available), it will override the temperature set above.
thickness	float	0	Surface thickness, sets component volume per thickness*area for Fang model
volume	float	0	Alternate way for setting volume directly
charge_density	float	0	Surface charge density, in C/m <sup>2</sup> .

transparency	float	0	Assigns fraction of particles that can pass through the component without hitting it. Useful for modeling meshes. Valid entries are 0 (opaque) to 1 (fully transparent).
c_stick	tuples	-1	Sets default sticking coefficient for the component group, negative value indicates to use other (temperature based) model for surface deposition
c_outgas	float	1	Scales diffusion coefficient
c_rest	float	1	Sets default coefficient of restitution, which controls velocity of reflected particulates
c_accom	float	1	Sets default coefficient of thermal accommodation, 0 leads to fully specular, 1 fully diffuse reflection
sm_A_ham	float	1.31e-19	Data for Hamaker particle adhesion model, Hamaker constant, J
sm_H0	float	0.3e-9	minimum contact distance, 0.3 nm
sm_rms1	float	4e-9	rms term 1 for surface roughness
sm_rms2	float	2e-9	rms term 2 for surface roughness
sm_lambda1	float	111e-9	spacing between undulation 1
sm_lambda2	float	250e-9	spacing between undulation 2
centroid	float3		Centroid to use for torque calculation
<b>Example</b>			
surface_props{comps:[/detector_.*/,wall], temp:[300@0,300@5,100@5.5]}			

**II.f.15) SURFACE\_TRANSFORM**

Applies transformation to surface nodes

Key	Type	Default	Description
surface	string		Surface to apply transformation to. If not specified, the latest added surface will be used.
op	string		One of [reset, scale, rotate_x, rotate_y, rotate_z, translate]. Reset op marks the starting node for the transformation. Remaining operations will operate on nodes added after "reset". The rotate ops perform rotation about the specified axes.
angle	float	0	Rotation angle in degrees for rotate_x/y/z
offset	float3	[0,0,0]	Vector offset for translate.
factor	float	1	Scaling factor for scale. Node positions are multiplied by this value.
<b>Example</b>			
<pre>surface_load_unv{file_name:"satellite.unv",surface:sat} surface_transform{op:rotate_x,angle:90} surface_transform{op:translate,offset:[-0.6,3.223,-0.6]}</pre>			

## II.g) Sources

These ops load initial surface molecular and particulate contamination, and also include additional sources that continuously inject material into the domain.

### II.g.1) DETACH\_PARTICULATES

Releases surface particles generated by LOAD\_FIBERS or LOAD\_PARTICULATES. Supports two models: CONST and KLAVINS. With Const, each particle has some user-specified probability of being released. With the Klavins model, release probability is based on a local acceleration per paper by Klavins and Lee.

Key	Type	Default	Description
comps	s_list		Surface mesh component to associate the source with
release_model	string	Klavins	Release model, one of [KLAVINS, CONST]. The constant model releases a constant fraction of particles. The Klavins model uses the Klavins-Lee expression to compute the release fraction.
release_fraction	float	0.1	Release fraction for the constant model
accel_mag	float	0	If positive, uses this value to determine detachment probability in the Klavins and Lee model. Otherwise, uses $a=F/m$ where $F$ is the external force at the particle location.
release_interval	int	0	Time, in seconds, over which the particles should be released, or 0 to release all on the first time step.

#### Example

```
load_particulates_1246{comp:fairing, mat:flakes, parts_per_bin:100, level:500, C:0.926,
model:klavins, accel_mag: 73.6, release_interval:90}
```

### II.g.2) LOAD\_FIBERS

Generates fibers at a prescribed surface density. Fiber sizes are generated by sampling a random length and a random aspect ratio in the given limits.

Key	Type	Default	Description
comps	s_list		Surface mesh components to associate the source with
mat	string		Material to inject
size_range	float2	[1e-3, 2.5e-3]	Minimum and maximum fiber length
ar_range	float2	[20, 120]	Minimum and maximum fiber aspect ratio
vel_range	float2	[0.001, 0.01]	Initial velocity magnitude, m/s
surf_den	float	2000	Surface density in $\#/m^2$ of physical fibers to generate
particle_count	int	1000	Number of simulation particles to generate
detach_vel	float	0.01	Detachment velocity (m/s)

#### Example

```
load_fibers{comps:[top,bottom],mat:dust,ar_range:[50,200], surf_den:2000}
```

### II.g.3) LOAD\_GRAINS

Generates random surface objects meant to represent dust grains. The generated grains are automatically added to the surface dynamics collection, and hence respond to external forces such as gravity.

Key	Type	Default	Description
comps	s_list		Surface mesh components to use for the starting surface
mat	string		Material to inject
prefix	string	grain	Generated surfaces are named "prefix_XXX" where XXX is a number
size_range	float2	[1e-3,2.5e-3]	Grain min and max length for uniform sampling
ar_range	float2	1	Aspect ratio (L/D) range
vel_range	float2	0	Initial velocity magnitude range
h_range	float2	0.01	Range of min and max distance above the surface componen
shape	string	wedge	One of WEDGE (back to back pyramid) or ROCK (rock-like shape)
num_grains	int	0	Total number of particles to load
number_den	float	0	Number of particles per $m^2$ , alternative to num_grains

#### Example

```
load_grains{comps:aplate, mat:regolith, prefix:grain, shape: rock, h_range:[0.0008,0.0008],
size_range:[50e-6,200e-6], ar_range:[1,10.0], vel_range:[0.0,0.0], num_grains: 100}
```

#### II.g.4) LOAD\_MOLECULES [DEMO]

Adds molecular contamination to specified components. Contamination is set by specifying composition of volatile species trapped within the bulk material and the composition of a surface film. The actual outgassing is handled by SOURCE\_OUTGASSING.

Key	Type	Default	Description
comps	s_list		The component these properties should be applied to. Can use RegEx wrapped in <code>./</code> (such as <code>./</code> to match all components).
trapped_mats	s_comp		String list of materials trapped in the component with optional fractions, such <code>[0.9*hc, 0.1*n2]</code> or just <code>"hc"</code> for homogeneous composition.
trapped_mass	float	0	Mass in kg of outgassing material trapped in the component
surf_mats	s_comp		String list of materials making up the surface layer
surf_h	float	0	Height, in meters, of a surface layer
surf_mass	float	0	Mass of contaminant surface layer, alternative to <code>surf_h</code>

#### Example

```
comp_props{name:./, mat:al, trapped_mass:0, temp:300, mass_flux:0}
comp_props{name:harness, mat:al, trapped_mass:1e-4, trapped_mats:[0.6*hc1, 0.3*hc2, 0.1*n2],
surf_h:0, surf_mat:hc1, temp:350}
comp{name:scav, mat:al, trapped_mass:0, temp:[300@0,300@5,100@5.5]}
```

#### II.g.5) LOAD\_PARTICULATES\_1246

Generates particles according to the IEST-STD-1246D model. Particles are created by sampling size from uniform distribution in `[1,max_size]`. Macroparticle weight for each particle is then set such that the analytical PAC is recovered. Particles are then randomly redistributed to surface elements according to area ratio. This approach is more noisy than the prior per-element versions but decouples the surface mesh resolution from the particle count.

Key	Type	Default	Description
comps	s_list		Surface mesh component to associate the source with
mat	string		Material of the particulates
particle_count	float	0	Number of simulation particles to generate across all elements
particles_per_element	float	0	Number of particles to create per element, alternative to <code>particle_count</code>
level	float	500	IEST-STD-1246 level (largest particle per $0.1\text{m}^2$ )
slope	float	0.926	IEST-STD-1246 distribution slope, 0.926 per standard, 0.3-0.4 typical for surfaces exposed for a prolonged period
max_size	float		If specified, controls the maximum particle size in micron to sample. Otherwise, defaults to <code>level*1.2</code>
detach_vel	float	0.01	Detachment velocity, m/s

#### Example

```
load_particulates_1246{comps:fairing, mat:flakes, particle_count:20000, level:500, C:0.4}
```

#### II.g.6) LOAD\_PARTICULATES\_TAPELIFT

Generates particles according to tape lift data. The input consists of two vectors. The first one is the particle size in micrometer, and the second is the number of particles in the bin.

Key	Type	Default	Description
comps	s_list		Surface mesh components to associate the source with
mat	string		Material to inject
particle_count	int	10000	Number of simulation particles to generate
bins	f_list		Particle bin bounds, counts per $0.1\text{m}^2$
counts	f_list		Number of particulates in each bin. The length must be one less than the length of bins.
detach_vel	float	0.01	Initial velocity

#### Example

```
load_particulates_tapelift{comp:fairing, mat:flakes, bins:[10,25,100,250,500], counts:
[1000,800,100,10]}
```

II.g.7) SOURCE_COSINE [DEMO]			
Samples uniform speed particles with velocity direction following the cosine law			
Key	Type	Default	Description
comps	s_list		Surface mesh components to associate the source with
mats	s_comp		List of materials to inject. Can specify a single material, or a list with relative fractions.
Q	float	0	Volumetric flow rate in m <sup>3</sup> /s at 1atm and 293.15K
mass_flux	float	0	Mass flux in kg/m <sup>2</sup> /s
mdot	float	0	Mass flow rate in kg/s. Either Q, mass_flux, or mdot need to be specified.
v_drift	float		Source drift velocity
temp_range	float2	[-1,-1]	Optional temperature range for applying this source only to elements within the bounds (inclusive)
normal_emission	bool	false	If true, molecules will be injected in normal direction instead of sampling Lambertian vector
arrhenius_T_ref	float	0	If positive, flux will be scaled by $\exp(-E_a/RT)/\exp(-E_a/RT_{ref})$ , where $E_a$ is the source material activation energy
max_T	float	0	maximum surface temperature for Arrhenius scaling
start_ts	int	0	Time step to start the particle injection
stop_ts	int	-1	Time step to end the particle injection if >0
normal_emission	bool	false	If true, all mass will be generated in the normal direction
Example			
source_cosine{comps:bottom, mats:hcl, mass_flux:1e-6, v_drift:100, stop_ts:100}			

II.g.8) SOURCE_DESORPTION [DEMO]			
Enables desorption of surface-deposited material. This source is added automatically if not explicitly included.			
Key	Type	Default	Description
first_time_only	bool	false	Performs desorption only on the first call. This should be enabled for sequence simulations utilizing SCALE_OUTGASSING. If true, desorption time step will be set to the total simulated time (dt * num_ts). Otherwise, desorption performed at each time step using simulation dt.
first_time_only	bool	false	If true, all desorption will happen on the first time step with time interval controlled by dt_integrate. Otherwise, desorption through simulation time step size dt will be applied every time step.
dt_integrate	float	0	Time interval used in evaluation in the amount of desorbed mass, if zero, total simulated time (dt*num_ts) will be used. Applicable only if "first_time_only" is true.
Example			
source_desorption{first_time_only:true}			

II.g.9) SOURCE_DROPLET			
This source attempts to approximate a liquid droplet jet injected to vacuum. It is a very simplistic model and based on visual observations of such jets. It injects particles with uniform velocity but after some distance from the source, the velocities are perturbed by a small offset to model the jet break up.			
Key	Type	Default	Description
comps	s_list		Surface mesh injection component
mats	s_comp		Particulate materials to inject
diam	float2	[50e-6,250e-6]	Range of droplet radii in m
mdot	float	1e-6	Injection mass flow rate in kg/s
vel	float	10	Initial injection velocity, m/s
temp	float	293	Droplet temperature in K
dispersion_r	float	0.1	Distance in m at which velocities will be perturbed
dispersion_vel	float	0.1*vel	Magnitude of velocity perturbation
start_ts	int	0	Starting time step for source injection
stop_ts	int	-1	Ending time step for source injection, or -1 to run forever

**Example**

```
source_droplet{comp:inlet, mdot:2.5e-4, mats:[co2], temp:253, vel:20, diam:[50e-6,250e-6],
dispersion_r:0.08, dispersion_vel:0.5,stop_ts:3000}
```

**II.g.10) SOURCE\_EROSION**

This source models mass generation due to kinetic bombardment sputtering. **IN DEVELOPMENT.**

Key	Type	Default	Description

**Example****II.g.11) SOURCE\_EVAPORATION**

This source can be coupled with the above droplet source to convert liquid droplets to gaseous molecules. It utilizes the Hertz Knudsen model to determine the evaporation rate at a given droplet temperature. It can be optionally coupled with a Shin model to model droplet cooling [4].

Key	Type	Default	Description
source_mat	string		Particulate material of the droplets
target_mat	string		Molecular material into which gaseous molecules are added
alpha	float	0.65	Coefficient of Hertz Knudsen model
shin_model	bool	false	Controls whether the model of Shin should be used to model droplet cooling.
antoinie_coeffs	float3		A,B,C for Antoine vapor pressure equation, $P_v=10^{(A-B/(T+C))}$

**Example**

```
source_evaporation{mats:n2h4,alpha:0.65,shin_model:true}
```

**II.g.12) SOURCE\_MAXWELLIAN**

Injects particles with velocity sampled from the Maxwellian velocity distribution function

Key	Type	Default	Description
comps	s_list		Surface mesh components to associate the source with
mats	s_comp		List of materials to inject. Can specify a single material, or a list with relative fractions.
Q	float	0	Volumetric flow rate in m <sup>3</sup> /s at 1atm and 293.15K
mdot	float	0	Mass flow rate in kg/s.
mass_flux	float	0	Mass flux in kg/m <sup>2</sup> /s
num_den	float	0	Number density (#/m <sup>3</sup> ), only one of these four options can be specified.
temp	float		Maxwellian source temperature in K
v_drift	float	0	Source drift velocity
start_ts	int	0	Time step to start the particle injection
stop_ts	int	-1	Time step to end the particle injection if >0

**II.g.13) SOURCE\_OUTGASSING [DEMO]**

Turns on material outgassing. The actual amount generated is controlled by surface molecular loading specified by LOAD\_MOLECULES and material coefficients given by MATERIAL\_INTERACTION.

Key	Type	Default	Description
comps	s_list	*	Surface components to apply the source to
model	string	POWER	Material desorption model controlling mass generation. The options include [POWER, FANG, TABULAR, NONE]. These models are described in the Governing Equations section. The specified model has no impact on surface desorption. Setting model to NONE is analogous to running with POWER model and having no trapped materials. Fang model requires non-zero surface zone thickness.
file_name	string		CSV file containing tabular data, first row columns [1,2,...] indicate temperatures, subsequent rows column 0 is time, and the columns [1,2,...] are the data values for that time

data_type	string		One of [FLUX, PERCENT_TML], specifies type of data stored in the tabular file
time_unit	string	s	One of [s,m,h,d], time unit for tabular file
data_scale	float	1.0	Scaling for tabular data
exact	bool	false	Controls whether particles with fractional material specific weight should be created. <b>True</b> implies that mass will be conserved exactly at each time step but the simulation may end up with a large number of particles as at least 1 will be created from each outgassing surface element per time step. <b>False</b> results in particles created using a stochastic method such that mass is conserved only on average.
desorb	bool	false	Controls whether material is desorbed directly to gas phase instead of being added to the surface layer
start_ts	int	-1	Starting iteration for mass diffusion if >=0
stop_end	int	-1	Ending iteration for mass diffusion if >=0

**Example**

```
source_outgassing{exact:false}
```

tabular file format:

```
-1, T0, T1, T2, ...
```

```
t0, v0, v1, v2, ...
```

```
t1, v0, v0, v2, ...
```

**II.g.14) SOURCE\_PARTICULATE\_14644**

This source models particulates embedded in a gas flow with following the ISO-14644-1 clean room standard. The maximum concentration of particles ( $\#/m^3$ ) is given by  $C_N = 10^N (0.1/D)^{2.08}$  where  $N$  is the "ISO class".

Key	Type	Default	Description
comps	s_list		Surface component from where particles are injected
mats	s_comp		List of materials to inject. Can specify a single material, or a list with relative fractions.
flow_rate	float		Volumetric flow rate of the background gas, $m^3/s$
flow_speed	float		Flow velocity, controls the drift speed of the injected particles. m/s
v_sigma	float	0	Standard deviation for each velocity direction used to add a random Gaussian velocity component, m/s
particle_sizes	f_list	[0.1,0.2,0.3, 0.5,1,5]	Particle sizes to simulate in $\mu$ .
macroparticle_count	int	5*size(particle_bins)	Number of simulation particles to generate per time step. This number is divided evenly across all particle sizes. Higher number results in a decreased simulation noise but longer simulation times.
iso_class	float		ISO class N, valid range is [0.1:9]
exponent	float	2.08	Exponent used in the $C_N$ equation
start_ts	int	-1	Time step to start the source
stop_ts	int	-1	Time step to end the source

**Example**

```
source_particulate_14644{comp:inlet, mats:dust, iso_class:6, flow_rate:10,
flow_speed:1,v_sigma:0.1,stop_it:500}
```

**II.g.15) SOURCE\_PARTICULATE\_PPM**

This source models particulates embedded in a background flow, as may be the case with cleanrooms or ECS flow. Particulates are born with random size sampled from a distribution, and initial drift velocity in the surface normal direction. Velocity can also have optional random component sampled from the Gaussian distribution. Injection mass flow rate is obtained from  $\dot{m} = Q_{flow} \rho_{flow} (ppm)_m \cdot 10^{-6}$ . The source samples the specified number of simulation particles per time step per component (the particles are assigned simulation specific weight to satisfy the injection mass).

Key	Type	Default	Description
comps	s_list		Surface component from where particles are injected
mats	s_comp		List of materials to inject. Can specify a single material, or a list with relative fractions.
ppm_mass	float		Parts per million, per mass.

flow_density	float		Mass density of the background gas, kg/m <sup>3</sup> .
flow_rate	float		Volumetric flow rate of the background gas, m <sup>3</sup> /s
v_drift	float		Drift velocity of the injected particles (physically should be the same as gas flow velocity), m/s
v_sigma	float	0	Standard deviation for each velocity direction used to add a random Gaussian velocity component, m/s
size_range	float2		[min,max] range for particulate sizes, $\mu$ m
size_dist	string	UNIFORM	Distribution method for size sampling, one of [UNIFORM,GAUSSIAN]
particle_count	int	10	Number of simulation particles to create per time step, per component
start_ts	int	0	Time step to start the source
stop_ts	int	-1	Time step to end the source
<b>Example</b>			
<pre>source_particulate_ppm{comp:inlet, mats:dust, ppm_mass:1, v_drift:2, v_sigma:0.1, size_range: [1,10], size_dist:gaussian,start_ts:0, stop_ts: 500, flow_rate:10,flow_density:1.18, particle_count: 5}</pre>			

**II.g.16) SOURCE\_PLUME**

Projects analytical plume per the model of Woronowicz [5]. This source computes surface flux to target components and also sets volume mesh density for visualization. No particles are generated. The source does not consider re-emission and only direct line of sight is considered.

Key	Type	Default	Description
comps	s_list		Source components, will generate plume from each surface element centroid
comp_ave	bool	false	Use average centroid and direction of specified component elements, or assign individual sources to each
offset	double	0	Displacement of source in normal direction if comp_ave=true
mats	s_comp		List of materials to inject.
x0	float3		Alternatively, can provide position and direction for the plume
dir	float3		Plume direction if component not specified
temp	float		Plume temperature in K
ue	float		Plume mean velocity in m/s
mdot	float		Flow rate in kg/s
start_ts	int	0	Time step to start the source
stop_ts	int	-1	Time step to end the source
<b>Example</b>			
<pre>source_plume{comps:inlet, mdot:0.5e-4, mats:[co2], temp:273, ue:20, start_ts:0, stop_ts:3000}</pre>			

**II.g.17) SOURCE\_POINT**

Models a point source using the effusion algorithm per Appendix B in Koo thesis [6]

Key	Type	Default	Description
pos	float3		Source position
dir	float3		Injection direction
mats	s_comp		List of materials to inject.
model	string		Time decay model, one of [EXP,CONST]
temp	float		Effusion temperature in K
v_drift	float	0	Drift velocity in the normal direction
mdot	float		Flow rate in kg/s
tau	float		Time constant for EXP model in hours, mdot = mdot0*exp(t/tau)
start_ts	int	0	Time step to start the source
stop_ts	int	-1	Time step to end the source
<b>Example</b>			
<pre>source_point{}</pre>			



**II.g.18) SOURCE\_RADIATION**

This source attempts to compute heat flux from a volume plume onto source components. It works by looping over all mesh nodes, and in each cell of sufficient density and temperature, constructing a ray from the cell centroid to all surface triangle centroids. The element's heat flux is incremented assuming  $1.5kT \cdot \text{den}$  source rate decaying with  $r^2$ .

Key	Type	Default	Description
source_mats	s_list		List of materials contributing to radiation heat flux
nd_min	float	1e14	Minimum number density for calculation to proceed
temp_min	float	1000	Minimum temperature

**Example**

```
source_radiation{mat:photon,source_mats:[n2], temp:1e5}
```

**II.g.19) SOURCES\_CLEAR**

Deletes all sources

Key	Type	Default	Description

**Example**

```
sources_clear{}
```

## II.h) Surface Output

The following operations are used to write out the surface mesh. Some formats support only the shape information (STL, UNV, etc.) and hence are primarily useful for file conversion. For instance, a TSS-imported mesh can be exported in the UNV format for additional post-processing in Salome. Other writers (Tecplot, VTK) also include mesh-based simulation results. The Tecplot writer supports only the legacy format and is not as actively updated as the VTK writer. The VTK writer is recommended, with files then visualized in Paraview or VisIt. The table below lists the variables supported by the VTK writer. The Mat column indicates whether the variable is material-specific. Variables listed as M or P can be used to write out material data for molecular or particulate species. If the mat is omitted, the cumulative sum is saved. For example, "surf\_height.hc1" is the height of molecular film of material "hc1", while "surf\_height" includes all molecular species. Variable names can be pre-pended with "cv\_" to output coefficient of restitution in parallel runs.

Name	Mat	Units	Description
area	no	m <sup>2</sup>	Element area
normals	no	-	Surface element normal vectors (included by default)
node_id	no	-	Mesh node id
element_id	no	-	Mesh element id (included by default)
comp_id	no	-	Component group index (included by default)
temperature	no	K	Surface element temperature
mli_temperature	no	K	Temperature of MLI on each component, available only with TSS loader
charge_density	no	C/m <sup>2</sup>	Surface charge density
velocity	no	m/s	Velocity of the surface actor
heat_flux	no	W/m <sup>2</sup>	Total heat flux (for example from radiation source)
cv_*	-	-	(prefix), outputs coefficient of variation (standard deviation scaled by mean) for parallel runs
surf_mass	M	kg	Mass of the surface molecular film
surf_mass_rate	M	kg/s	Surface layer mass accumulation rate
mass_flux	M	kg/m <sup>2</sup> /s	Net mass flux to the surface
mass_flux_in	M	kg/m <sup>2</sup> /s	Incident mass flux
stuck_surf_h	M	A	Height of a permanently stuck molecular layer
normal_force	M/P	N	Force from impinging particles, computed using net momentum
surface_pressure	M/P	N/m <sup>2</sup>	Magnitude of surface pressure (net normal momentum flux) transferred to the surface
momentum_flux_in	M/P	kg/m/s <sup>2</sup>	Normal momentum flux of incoming particles, computed by dotting incident particle velocity with surface normal vector
momentum_flux_out	M/P	kg/m/s <sup>2</sup>	Normal momentum flux of bounced off particles, computed by dotting exiting particle velocity with surface normal vector
net_energy	M/P	J	Energy transferred to the surface from the difference between incoming and outgoing mass*velocity*velocity
net_energy_flux	M/P	J/m <sup>2</sup> /s	Energy flux transferred to the surface
incidence_angle	M/P	degree	Average off-normal angle for incoming particles
source_element	M/P		The source element for the majority of incoming particulates. Not yet supported for molecular materials.
source_fraction	M/P		Fraction of incoming particulates that came from the "source_element" element.
sun_view	-	bool	Indicates whether the element has a view to the sun. Only for TSS surfaces.
sub_div	-	-	TSS element subdivision id
back_face	-	bool	0/1 value indicating whether the element is the backface of a TSS surface
surf_height	M	A	Height of a surface molecular film for a species or all cumulative
surf_height_rate	M	m/s	Surface layer height accumulation rate
trapped_mass	M	kg	Mass of the trapped materials in the material substrate layer
trapped_mass_rate	M	kg/s	Rate of mass change in the material substrate layer
PAC	P	%	Percent area coverage in % (0.1 is 0.1% not 10%)
level	P	-	Non-dimensional particulate level computed from PAC assuming C=0.926.

**II.h.1) SURFACE\_SAVE\_CSV**

Writes the surface data in a .csv format. Outputs element ids, back side flag, and the deposited surface height for all materials. Outputs data only for the specified surfaces and matching components.

Key	Type	Default	Description
file_name	string		Saves in "results/"+file_name.csv
surface_names	s_list	*	List of surfaces to output
comps	s_list	*	List of components to output
skip	int	-1	Frequency of saves

**Example**

```
surface_save_csv{file_name:deposition}
```

**II.h.2) SURFACE\_SAVE\_STL**

Writes the surface mesh (without any element data) in the STL format. Quads are broken down to two triangles.

Key	Type	Default	Description
file_name	string		Saves in "results/"+file_name
surface_names	s_list	*	List of surfaces to output
comps	s_list	*	List of components to limit the output to
skip	int	-1	Frequency of saves

**Example**

```
surface_save_stl{file_name:"surf.stl"}
```

**II.h.3) SURFACE\_SAVE\_TECPLOT**

Saves the surface mesh and associated data in legacy Tecplot ASCII format. Outputs molecular height, and particulate levels, PAC. This function is retained for legacy reasons, but for full output functionality, it is recommended to use VTK output.

Key	Type	Default	Description
file_name	string		Saves surface file in "results/"+file_name
surface_names	s_list	*	List of surfaces to output
comps	s_list	*	List of components to limit the output to
skip	int	-1	Frequency of surface saves.

**Example**

```
surface_save_tecplot{file_name:"surf.dat"}
```

**II.h.4) SURFACE\_SAVE\_UNV**

Writes the surface mesh only (no data) in the UNV format

Key	Type	Default	Description
file_name	string		Saves in "results/"+file_name
surface_name	string		Surface to output, if not specified, the last surface added will be selected.
skip	int	-1	Frequency of saves

**Example**

```
surface_save_stl{file_name:"surf.unv"}
```

**II.h.5) SURFACE\_SAVE\_VTK [DEMO]**

Saves the surface mesh and corresponding surface properties in a VTK format, which can be visualized with Paraview or Visit. If called prior to starting a simulation run (run\_sim), this prop will add a run time diagnostic which results in a file output every "skip" time steps. Otherwise, if called after simulation finishes, it saves current data.

Key	Type	Default	Description
file_name	string		File name prefix, will save in "results/"+file_name+".vtp"
skip	int	-1	Frequency of surface saves.
format	string	binary	One of [ASCII, BINARY]. Binary data is base64-encoded.
surf_names	s_list	*	List of surfaces to output

comp_names	s_list	*	Component names to output
save_frames	bool	true	Controls whether time step should be appended to file name, which results in individual file for each output to make animations. Setting to false will overwrite the existing file to save hard drive space.
vars	s_list		List of variables to output. See top of the section for the available list. Only the surface mesh geometry is saved if vars empty
start_ts	int	-1	First time step at which output should begin
end_ts	int	-1	Time step at which output ends
skip	int	100	Number of time steps between outputs

**Example**

```
#save multiple files 100 time steps apart
surface_save_vtk(skip:100,file_name:"surf",vars:[surf_h.hcl,trapped_mass])
run_sim()
#save the final results
surface_save_vtk(file_name:"surf_final",vars:[surf_h.hcl,trapped_mass], format:ascii)
```

## II.i) Particle Output

These operations are used for saving particle traces and random samples for post processing.

II.i.1) PARTICLE_SAVE_TECPLOT			
Saves particles in Tecplot format			
Key	Type	Default	Description
file_name	string		Output file name
start_ts	int	0	First time step for output
end_ts	int	-1	Last time step for output
skip	int	100	Number of time steps between saves
Example			
particle_save_tecplot{file_name:"particles.dat"}			

II.i.2) PARTICLE_SAVE_VTK [DEMO]			
Saves a random subset of particles in the VTK format.			
Key	Type	Default	Description
file_name	string		Saves in "results/"+file_name+".vtp"
mat	string		Gaseous or particulate material to output
num_particles	int	1000	Number of particles to output
max_id	int	-1	Maximum particle id for picking the random particles, or -1 to use all available particles.
start_ts	int	-1	First time step at which output should begin
end_ts	int	-1	Time step at which output ends
skip	int	100	Number of time steps between outputs
Example			
particle_save_vtk{file_name:"particles",mat:flakes,skip:10,num_particles:2000}			

II.i.3) PARTICLE_SAVE_HISTOGRAM			
Saves a histogram of particle sizes on the specified surface components. Data is stored in .csv format, with columns corresponding to the number of real and simulation particles in the x[i]-x[i+1] bin. Optionally, a species-level breakdown is possible and data can be normalized by area.			
Key	Type	Default	Description
file_name	string		Saves in "results/"+file_name+".csv"
comps	s_list	*	List of component names, supports regex within slashes
mat	string		Optional material to limit output to
bins	f_list	[1,10,25,50,100,150,250,500,750,1000,2500]	Histogram bin bounds
el_file_name	string		If set, will output a file containing ids and fractions for up to 10 elements from which particles came from for each target element id
save_frames	bool	true	Controls whether individual files should be written for animation (true) or the file should be overwritten to save space (false)
start_ts	int	0	First time step for file output
end_ts	int	-1	Last time step for file output
skip	int	100	Number of time steps between saves
per_01m2	bool	false	If true, data will be normalized to counts per 0.1m <sup>2</sup>
Example			
particle_save_histogram{file_name:hist,comps:[source,floor],per_01m2:true,skip:1000}			

II.i.4) PARTICLE_TRACE [DEMO]			
Saves position and other data for one or more particle at each time step. Saves in VTK format.			
Key	Type	Default	Description
file_name	string		Saves in "results/"+file_name+".vtp"
mat	string		Gaseous or particulate material to output

num_traces	int	0	Number of particles to trace. Alternative is to specify ids directly.
max_id	int	-1	Maximum id for generating random trace ids if num_traces is specified
ids	i_list		List of particle ids to trace
skip	int	-1	Frequency in time steps of file saves. -1 saves only at end.

**Example**

```
particle_trace{file_name:trace,mat:flakes,num_traces:100,max_id:28736}  
particle_trace{file_name:trace,mat:hcl,ids:[250,1050,1007]}
```

## II.j) Volume Mesh

These operations control the creation and export of an optional volume Cartesian mesh. The following variables are currently supported. Macroscopic fluid properties such “nd” (for number density) can be appended with a “.mat” to limit the output just to that flying material, i.e. nd.water. However, this option is available only if the material is created with “compute\_fluid\_properties” enabled, which is disabled by default to save memory. Without the dot, the fluid properties output the total values across all species, i.e. “nd” is the combined number of atoms/molecules per volume across all flying materials. Variable names can be pre-pended with “cv\_” to output coefficient of restitution in parallel runs.

Name	Mat	Units	Description
nd	yes	#/m <sup>3</sup>	Number density (molecules per cubic meter)
u	yes	m/s	Species mean velocity vectors
t	yes	K	Species temperature from Maxwellian distribution
mpc	yes	-	Number of simulation particles per cell
cell_vol	no	m <sup>3</sup>	Cell volume
pressure	no	Torr	Total pressure from partial pressure sums per $p=nkT/133.32$
flow_vel	no	m/s	Loaded flow velocity vectors, available only flow loaded with “use_volume_grid”
flow_rho	no	kg/m <sup>3</sup>	Loaded flow number density as given or computed from ideal gas law

### II.j.1) VOLUME\_MESH [DEMO]

Generates an optional volume Cartesian mesh. CTSP will then compute bulk gas properties such as density and pressure. These can be useful for visualization of contaminant plumes. Volume mesh also specifies a bounding box for removing particles.

Key	Type	Default	Description
dx	float		Approximate cell spacing in x direction
dy	float		Approximate cell spacing in y direction
dz	float		Approximate cell spacing in z direction
xmin	float3		Optional xmin coordinate of mesh bounding box. If not specified, surface mesh bounding box is used.
xmax	float3		Optional xmax coordinate of mesh bounding box. If not specified, surface mesh bounding box is used.
expand	f_list	0	By default, the volume mesh bounds are identical to the surface bounding box. This option allows for the bounds to be expanded. There are three options: a) single value results in uniform offset added to all 6 faces, b) three values add the same offset to +/- X,Y,Z faces, and c) six values provide specific offset for each [-X,+X,-Y,+Y,-Z,+Z] dimension.
max_refinement	string	3	Specifies maximum possible refinement level, needed to initialize data structures.
symmetry	s_list		Valid values are [X,Y,Z]. Applies symmetry in the specified dimension(s).
allow_large_mesh	bool	false	Needs to be set true to allow running with more than 400x400x400 mesh nodes. Acts as a safety valve.

#### Example

```
volume_mesh{dx:0.01,dy:0.02,dz:0.01,expand:0.01}
volume_mesh{dx:0.1,dy:0.1,dz:0.1,expand:[0.1,0.1,0.5], symmetry:[X,Y]}
```

### II.j.2) VOLUME\_MESH\_REFINE

Adds mesh refinement over a specified bounding box. Particularly useful for running DSMC simulations.

Key	Type	Default	Description
type	string	box	Specifies refinement type, currently only BOX is supported
level	int	1	Level to refine to, original mesh is level 0, each level splits cells into 8 octants
xmin	float3		Minimum extent for the BOX refinement type
xmax	float3		Maximum extent for the BOX refinement type

#### Example

```
volume_mesh_refine{type:box, level:1, xmin:[0.1,0.1,0.1], xmax:[0.2,0.4,0.3]}
```

**II.j.3) VOLUME\_SAVE\_TECPLOT**

Saves the volume mesh and corresponding data in a Tecplot format. Data is averaged between saves. Legacy function, currently supports only uniform mesh.

Key	Type	Default	Description
file_name	string		File name, results saved in "results/"+file_name
vars	s_list		List of variables to output. Some options include "nd.fm, u.fm, t.fm, pressure", where "fm" is name of a flying material.
start_ts	int	-1	Starting time step for diagnostic output
end_ts	int	-1	Ending time step for diagnostic output
skip	int	-1	Frequency of file saves for diagnostic output

**Example**

```
volume_save_tecplot{skip:2000,file_name:"field.dat",vars:[nd.hcl]}
```

**II.j.4) VOLUME\_SAVE\_VTK [DEMO]**

Saves the volume mesh and corresponding data in a VTK format. Data is averaged between saves. When generating animations, it is possible to get less noisy data without using more particles by saving less frequently. Data is saved as VTK Image File (.vti, uniform Cartesian mesh) if the volume mesh is not refined, otherwise it is saved as VTK Structured Grid (.vts). Prior to 1.9.9, data was stored as "node centered" (point data), however the current version stores data using cell centered convention.

Key	Type	Default	Description
file_name	string		File name, results saved in "results/"+file_name+".vt?"
vars	s_list		List of variables to output. Some options include "nd.fm, u.fm, t.fm, pressure", where "fm" is name of a flying material.
skip	int	-1	Frequency of file saves
format	string	binary	One of [ASCII, BINARY]. Binary data is base64-encoded.
save_frames	bool	true	Controls whether time step should be appended to file name
start_ts	int	-1	Starting time step for diagnostic output
end_ts	int	-1	Ending time step for diagnostic output
skip	int	-1	Frequency of file saves for diagnostic output

**Example**

```
volume_save_vtk{skip:2000,file_name:"field",vars:[nd.hcl,pressure,t]}
```



### III. Governing Equations

#### III.a) Molecular Contamination

Molecular outgassing arises from volatile gases trapped inside the material diffusing to the surface and desorbing into the gas phase. The diffusion rate between the bulk and the substrate, and the desorption to the gas phase is a function of concentration gradients and surface temperature. The model in CTSP attempts to capture this basic physical process. As plotted in Figure 10, all surface objects are assumed to consist of a native solid substrate containing an arbitrary heterogeneous mixture of trapped gases (region I). At the surface is a thin layer composed of an arbitrary combination of molecular species (region II). The surface layer can also contain particulates. Molecules and particulates can leave the surface layer and enter the gas phase (region III). Material in the gas cavity eventually encounters other geometry components (unless they leave the computational domain through open boundaries) and possibly adsorbs to that component surface layer. Molecules can also migrate from the surface back to the substrate. For generality, we also allow the surface to generate additional material according to some prescribed flux, as is the case with openings venting an internal cavity. This prescribed flux is also useful for representing objects for which a QCM-measured outgassing rate is available.

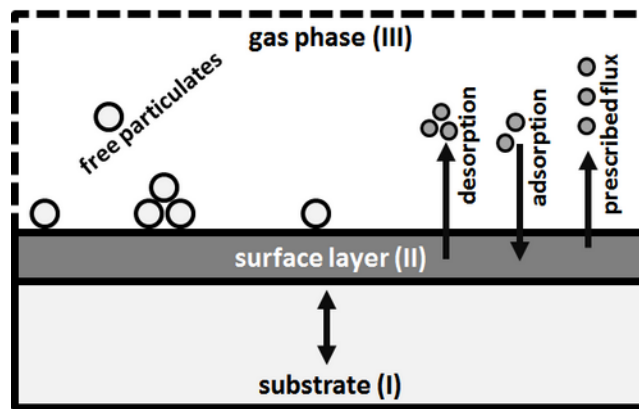


Figure 10. Overview of the surface model used by CTSP. All components are assumed to consist of a solid substrate containing some trapped contaminants and a surface layer in contact with the gas phase.

The initial composition of the substrate and surface regions is specified in the input file for each geometry component as illustrated below:

```
surface_props{comp:ebox, mats:ti, temp:[250@0,300@2,350@5]}
load_molecules{comp:ebox, trapped_mass: 1e-4, trapped_mats: [0.8*hc1,0.1*water,0.1*n2],
surf_h:5e-10, surf_mats:water}
```

The first command specifies the composition of the surface substrate (100% Titanium). It also specifies a time-varying component temperature. The next command load molecular contaminants into the substrate and the surface layer. Here the amount of trapped material is specified by providing the total weight of the contaminant population to be distributed across all surface elements of the listed component. The surface contamination is specified by listing the height of the surface layer. Properties for materials such as ``hc1" and ``water" need to be specified prior to this step. Migration of mass from the substrate to the surface layer is governed by molecular diffusion. CTSP implements two models. First, the code supports a simple power law commonly used by the contamination community [7],

$$\frac{dN}{dt} = C_{pow} N \exp\left(-\frac{(E_a)_{dif}}{RT}\right) t^k$$

where  $C_{pow}$  is a reaction constant,  $N$  is the number of molecules left in the substrate,  $(E_a)_{dif}$  is the activation energy for the diffusion process (in kCal/mol),  $R$  is the gas constant (in kCal/mol/K), and  $T$  is the component temperature (K). The coefficient for the time term  $t$  is taken to be  $k = -0.5$  for a diffusion-limited process. The reaction constant and

activation energy can be determined experimentally from the industry standard ASTM-E1559 test [8]. This exponential model does not support mass diffusion from the surface layer back to the solid material.

CTSP also implements a detailed model based on the work of Fang [9]. In their work, the authors put forth an analytical model for outgassing and contamination transport in a domain also consisting of a source solid material, a source layer, a cavity, and a target surface. An advection-diffusion model was used to treat the mass transport in the cavity and analytical model was utilized to capture the adsorption of gas material to the surface. These two processes are handled by the kinetic particles in CTSP. The concentration gradient in the solid region I is given by the diffusion equation

$$\frac{\partial n_c}{\partial t} = \nabla \cdot (D \nabla n_c) + f_1$$

Here  $n_c$  is the contaminant number density ( $\text{m}^{-3}$ ) inside the region I and  $D$  is the diffusion coefficient ( $\text{m}^2/\text{s}$ ). It is important to realize that computing the concentration gradient requires knowing the *volume* of the component, which is not available from the surface mesh data. Therefore, it is critical that component volumes are set appropriately using the SURFACE\_PROPS command.  $f_1$  is a source term allowing for additional contaminant generation. In our formulation, we set  $f_1 = 0$ . Integrating through a volume of the solid region, we have  $dN/dt = (\partial n_c / \partial n) A$ . Here  $N$  is the total number of contaminant molecules inside the solid region I,  $N = \int_V n_c dV$  and  $A$  is the area of interface between regions I and II.

The divergence theorem was used here, and we assumed that  $(\partial C / \partial n)$  is spatially uniform across the interface. All other boundaries are impermeable. This equation describes the number of molecules lost by the solid region. To satisfy mass conservation, it also governs the number of molecules gained by the surface layer. The surface layer is also incremented by adsorption of molecules from the gas phase and is similarly depleted by desorption of surface film into the gas phase. We label these two terms  $\Gamma_a$  and  $\Gamma_d$ . The time evolution of the surface number density  $\theta (\text{m}^{-2})$  is thus given by

$$\frac{\partial \theta}{\partial t} = -D \left( \frac{\partial n_c}{\partial n} \right) + \Gamma_a - \Gamma_d$$

We next assume that the concentration gradient  $-(\partial n_c / \partial n)$  is proportional to the amount of material inside and on the surface of the object. We define a sorption function  $H(n_c, \theta)$  such as

$$-\frac{\partial n_c}{\partial n} = H(n_c, \theta) = n_c - \gamma \theta$$

Here  $\gamma$  ( $\text{m}^{-1}$ ) is an "equilibrium partition coefficient" such that at equilibrium  $n_c = \gamma \theta$ . We thus have  $d\theta/dt = D(n_c - \gamma \theta) + \Gamma_a - \Gamma_d$ . From this expression we see that at equilibrium we also require  $\Gamma_a = \Gamma_d$ . Satisfying this requirement is demonstrated in Example 1. The desorption flux is given by  $\Gamma_d = \theta_1 / \tau_r$  where

$$\tau_r = \tau_0 \exp \left( \frac{(E_a)_{des}}{RT} \right)$$

is the molecular residence time. The parameter  $\tau_0$  is the vibrational period of the molecule with typical values around  $10^{13} \text{ s}$  [7] and  $(E_a)_{des}$  is the activation energy for the desorption process. The parameter  $\theta_1 = \min(\theta, \eta / (\pi r^2))$ , where  $\eta / (\pi r^2)$  is the maximum number of molecules per unit area. Here  $r$  is the molecular radius and  $\eta_0$  is a scaling "packing" factor. Both of these values are user parameters. This formulation limits the desorption rate to that corresponding to a fully occupied monolayer if surface film thickness exceeds a single monolayer. The adsorption flux  $\Gamma_a$  term is described in a subsequent section on particle impact.

The above algorithm is implemented numerically as follows. We loop through all surface elements. On each, we first use the exponential or the detailed model to compute the total number of molecules diffusing to (or from) the surface layer. Here the code takes into account the relative molar composition of materials in the substrate and the surface layer. Next, the appropriate number of molecules is transferred to (or from) the surface layer. Note, with the "power" model, there is no transfer from the surface to the bulk. We next compute the number of real molecules to desorb,  $N_d = (N_{surf}/\tau_r)\Delta t$ . The corresponding number of simulation particles is  $M = N_d/w_{mp}$ . Generally,  $N_d$  will not be evenly divisible by the macroparticle weight  $w_{mp}$ . The code supports two injection schemes. In the exact scheme, as many particles as possible will be created with the default  $w_{mp}$  and then an additional particle will be created with some fractional weight. The second stochastic approach does not create fractional weight particles but instead uses random numbers to create full weight particles with probability  $N_d/w_{mp}$ . This second approach is mass conserving only on average at steady state but avoids the excessive number of simulation particles that may result with the first exact model.

### III.b) Particulates

Just as with molecular contaminants, simulating particulate redistribution requires models for generation, transport, and deposition. Particulate contamination is traditionally divided into two categories: "standard" particulates and fibers. Fibers are particulates with aspect ratio  $AR \equiv l/d > 10$  [10]. Fibers can be characterized by specifying their count per unit area along with the observed size ranges. CTSP implements a source for fibers which generates the user specified surface concentration with lengths and aspect ratios sampled from the uniform distribution within the user specified limits. The model for the standard particulates is more involved, and is described next.

The contamination control community often uses the IEST-STD-1246D standard to describe the size variation of particulates on a surface [11]. This standard provides a cumulative distribution function for particle counts given by

$$\log_{10}(N_{cum}) = C(\log_{10}^2(L) - \log_{10}^2(l))$$

$N_{cum}$  is the total number of particulates with sizes greater or equal to  $l$  per 0.1 m<sup>2</sup> (prior versions of this standard used the same model but the count was per ft<sup>2</sup>). The particulate length  $l$  is given in micrometers. The parameter  $L$  is the surface cleanliness level and  $C$  is the "slope" of the distribution. The standard assumes  $C = 0.926$  for freshly cleaned surfaces, however real-world tape lifts indicate values closer to 0.4 [7]. Both  $C$  and  $L$  are user inputs.

We are generally more interested in the actual number of particulates of some size. This value can be approximated by subtracting two cumulative counts offset by 1  $\mu m$ ,

$$N = 10^{C(\log_{10}^2(L) - \log_{10}^2(l))} - 10^{C(\log_{10}^2(L) - \log_{10}^2(l+1))}$$

The distribution given by the above equation indicates that the concentration of particulates increases exponentially as the particle size decreases. However, small particles are also less likely to come off the surface due to an increased ratio of adhesion to detachment forces. Particles unable to detach do not contribute to contaminant redistribution. Determining what fraction of particles of some size  $l$  detaches remains a significant uncertainty in our model. In 1987, Klavins and Lee studied the problem of surface adhesion by applying static loads to a test sample placed in a centrifuge [12]. These measurements were performed at loads up to 10<sup>5</sup>g and showed large variation in the detachment probability between individual tests. This variation is expected, since probability that a particle detaches is strongly influenced by the local surface roughness, particle shape, and orientation. Environmental effects such as humidity or electrostatic charge also play a role. Hence, at best, only a simple macroscopic estimates of detachment probability  $\Phi$  can be made. The authors found it to follow

$$\phi = \left[ 1 + \left( \log \left( \frac{a_d}{a_m} \right) / (\sqrt{2}\sigma_0) \right) \right] / 2$$

where  $a_d$  is the applied acceleration and  $\sigma = 1.45$  is the standard deviation. The parameter  $a_m$  is the mean acceleration for 50% removal, and is given by  $(85.07/L)^{4.08}$  for particles smaller than 42  $\mu m$  and  $(52.37/L)^{13.6}$  otherwise<sup>2</sup>. The

<sup>2</sup>The exponents on these two expressions are switched in the reference paper due to an apparent type. The formula shown here is consistent with graphs in the paper.

distribution of particles released from the surface can then be obtained by multiplying the initial size distribution with the release probability,  $N\Phi$ . These expressions are visualized in Figure 11 for  $L=400$ ,  $C=0.926$ , and  $a=5$  g. As can be seen, the release model predicts all particles larger than  $100\ \mu\text{m}$  detach given the 5 g acceleration. On the other hand, the detachment probability is less than 30% for particles smaller than  $20\ \mu\text{m}$ . The light gray dashed line corresponds to the distribution that needs to be generated by the particulate source.

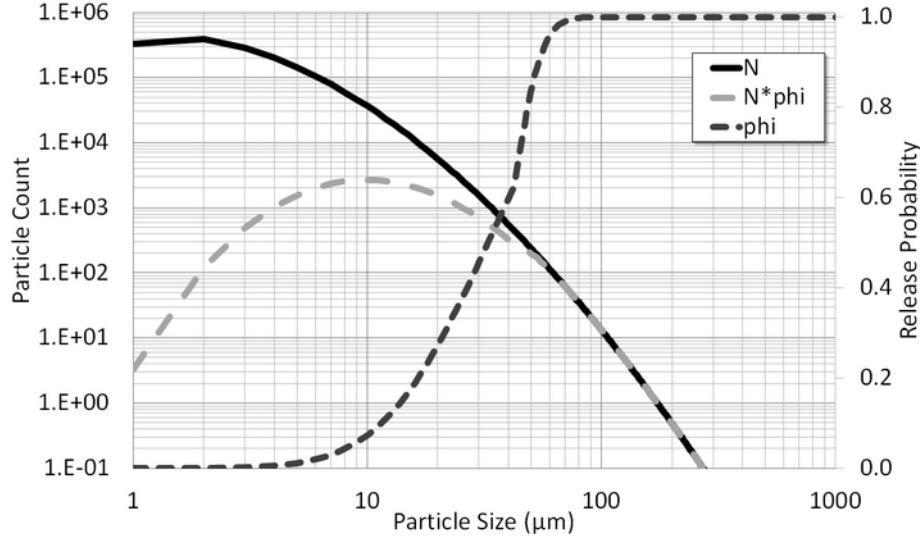


Figure 11. Particle counts, release probability, and the number of released particles for  $L=400$ ,  $C=0.926$  and  $a=5$  g.

For generality, we prefer to evaluate  $\Phi$  with  $a_d$  obtained from the sum of forces acting at the particle injection location. We can generate particles by sampling sizes from the IEST-STD-1246D distribution and for each compute the release probability. Without changes, this approach is however not practical. Considering  $L=400$  and  $C=0.926$ , we see that for every 200 micron particle, there are 13,079  $20\text{-}\mu\text{m}$  particles. We thus need to sample, on average, at least 13,079 particles per surface element to sample a single  $200\ \mu\text{m}$  particle. The dynamics of the large and small particles are sufficiently different making it important that all sizes are represented. We thus instead generate a constant number of simulation particles in each of the following bins:  $[1,10)$ ,  $[10,25)$ ,  $[25,50)$ ,  $[50,100)$ ,  $[100,250)$ ,  $[250, 500)$ ,  $[500,750)$ ,  $[750,1000)$  and use the macroparticle weight  $w_{mp}$  to recover the original distribution function. In each bin, particle sizes are sampled from the uniform distribution. This approach assures that the simulation contains a statistically significant number of particles off all sizes. Simulations presented in this report used 100 particles per bin for a total of 800 particles per surface element. All particle in a single bin share the same macroparticle weight. The weight is set such that the total percent area (PAC) coverage represented by the particles in the bins equals to the PAC given by the original distribution. In each  $[l_1, l_2)$  bin, we first sample  $N_p$  random sizes, and then compute

$$W \sum_p^{N_p} A_p = A_{ele} \sum_{l=l_1}^{l_2-1} N(l) A(l)$$

Here  $A_p$  is the cross-sectional area of  $p$ -th particle and  $A_{ele}$  is the surface area of the element.  $N(l)$  is given by the IEST-STD-1246D distribution equation and  $A(l)$  is the cross-sectional area of a particle of size  $l$ . For consistency, it is imperative that the same expression is used to compute  $A_p$  and the total distribution-based area. The aspect ratio  $AR = l/d$  varies with particle size. As summarized by Perry [13],

Particle size (microns)	Aspect Ratio
1-69	$AR = L^{0.1088}$

70-175	$AR = L^{0.8804}/26.53$
176-346	$AR = L^{2.589}/181500$
347+	$AR = L^{0.8964}/9.138$

The cross-sectional area is then  $A = d(l - d) + \pi d^2/4$ . The volume becomes  $V = (l - d)\pi d^2/4 + \pi d^3/6$ . The particle volume is used to set the mass from the material density,  $m = \rho V$ . Note that  $L$  corresponds to the cross-sectional area parallel to the particle long axis. For aerodynamic drag computations, we assume that the particle aligns with the flow so that  $A_d = (\pi d^2)/4$ .

Particles generated by the above algorithms are initially attached to the surface. The code next iterates over all particles and for each computes the detachment probability  $\Phi$  from the Klavins and Lee model or from a constant value specified by the user. The particle is detached if  $\Phi \geq R$ , where  $R$  is a random number. Otherwise, the particle cross-sectional area is used to update the source element percent area coverage. The model of Klavins and Lee does not offer any insight into detachment rate. It is not clear whether particles detach instantly or whether the detachment takes place over an extended period of time. The source model thus implements two schemes. In the first one, all particles able to leave do so at the first time step. The second approach models uniform detachment rate over a finite period of time. In this approach,  $\Phi/n_{it}$  is compared to  $R$ , with  $n_{it}$  being the number of time steps over which detachment is considered. The second approach is useful in simulations with time-varying gravitational or aerodynamic environments such as in the payload fairing during spacecraft launch.

### III.c) Particle Motion and Surface Impact

Once particles are generated by the respective sources, their positions are updated by numerically integrating  $d\vec{x}/dt = \vec{v}$ . Velocity is integrated from  $d(m\vec{v})/dt = \sum \vec{F}$  using either the second order Leapfrog method or the fourth-order Runge Kutta method.  $\sum \vec{F}$  is the sum of all forces acting on the particle and  $m$  is the particle mass. The total force acting on particles is  $\sum \vec{F} = \vec{F}_g + \vec{F}_d + \vec{F}_e + \vec{F}_r + \vec{F}_x$  where the terms correspond to gravitational, aerodynamic drag, electrostatic, solar radiation forces, and a general user defined external force. Orbital motion of the parent body can also be defined to model particulate return on orbit crossings. The following expressions are used to evaluate the forces:

$$\begin{aligned}
 \vec{F}_g &= m\vec{g} \\
 \vec{F}_d &= \frac{1}{2}\rho_g C_d A_d \frac{(\vec{v}_a - \vec{v}_p)^2}{|\vec{v}_a - \vec{v}_p|} \\
 \vec{F}_e &= q\vec{E} \\
 \vec{F}_r &= \frac{A_d E_f}{c} \frac{\vec{r}_s}{|\vec{r}_s|} \\
 \vec{F}_x &= \vec{F}_x(t)
 \end{aligned}$$

The drag force is computed using a drag coefficient for a flow past a sphere from the model of White [14],

$$C_d = \frac{24}{Re} + \frac{6}{1 + \sqrt{Re}} + 0.4 \quad Re < 2 \times 10^5$$

The Reynolds number is computed from  $Re = \rho_g u l / \mu$ , where  $\rho_g$  is the gas mass density,  $u$  is the magnitude of relative velocity between the particle and the ambient gas,  $l$  is the particle major length, and  $\mu$  is the dynamic viscosity of the gas.  $A_d$  is the cross-sectional particle area for drag computations. As mentioned previously, CTSP assumes that particles can be modeled as cylinders with spherical end caps, and thus  $A_d = \pi b^2/4$ , with  $b$  being the minor length (cross-section diameter). Additional work is needed to quantify the error introduced by using the sphere drag coefficient for particulate motion.

In the electrostatic Lorentz force,  $q$  is the particle charge and  $\vec{E}$  is the electric field. For molecular materials, charge is set directly in the input file. For particulates, we instead specify the surface charge density, and charge is then computed by multiplying through the particle total surface area,  $q = \sigma A_{tot}$ . The radiation pressure expression assumes the particle is uniformly spinning so the incidence angle can be averaged out and  $\vec{r}_s$  is a vector from the source to the particle. To improve performance, the code applies forces only if appropriate data are specified. For instance, gravitational force is considered only if the world acceleration vector  $\vec{g}$  is nonzero. Aerodynamic drag is computed only if  $\rho_g > 0$ . Intermolecular collisions in regimes outside the free molecular flow regime can also be modeled using the DSMC No Time Counter (NTC) scheme of Bird [3].

During each particle push the code checks for surface interaction. If the particle strikes a surface, an impact handler is used to determine whether the particle sticks to the surface, and if not, to set its post-impact velocity. Surface impact is the only part of the code where a different algorithm is applied to particulate and molecular contaminants. When a molecule impacts a surface, CTSP first determines the probability of the molecule striking the native material instead of another adsorbed molecule. This probability is given by  $P = N_2 \pi r^2 (\eta_0 A_{ele})$ , where  $N_2$  is the number of molecules adsorbed to the surface. CTSP then computes residence time using the previously noted equation at the temperature of the impacted surface element and appropriate activation energy. The molecule is re-emitted if  $\tau_r / \Delta t \geq R$  where  $R$  is a random number. In this sense,  $\tau_r / \Delta t$  is analogous to the sticking coefficient  $\alpha_{sc}$  commonly utilized in other mass transport codes. For generality, CTSP allows the user to define a fixed  $\alpha_{sc}$ , in which case the prescribed value will be used instead of the temperature-based model. For rebounding particles we first sample the new velocity magnitude  $v_t$  from the Maxwellian speed distribution function at the surface temperature. The particle's new speed is set to  $v + \alpha_a(v_t - v)$  where  $\alpha_a$  is the thermal accommodation coefficient. The new velocity direction follows the cosine law sampled according to a model of [3]. On the other hand, if  $\tau_r / \Delta t < R$ , the particle is adsorbed to the surface layer. Computationally, this involves removing the particle from the simulation and incrementing the surface count of particle's  $N\Phi$  by the particle specific weight  $w_{mp}$ . This term correlates to the adsorption flux,  $\Delta N_2 = \Gamma_a A_{ele} \Delta t$ . For post-processing, the surface layer molecular count can be converted to a thin film height by assuming spherical molecules,

$$h = N_2 \frac{(4/3)\pi r^3}{A_{ele}}$$

Different model is used for particulates. Particulate post-impact velocity is given by a user-defined coefficient of restitution,  $\alpha_r = v_2 / v_1$ . This parameter controls the "bounciness" of the particle. The particulate is allowed to leave until the post-impact velocity falls below some user defined threshold. The default value used in most of our simulations is 0.001 m/s. The mass of the particle is assumed to remain constant (i.e., the particle does not break up upon impact). Particles without sufficient post-impact velocity are deleted from the simulation and their cross-sectional area is used to update the target surface element percent area coverage,

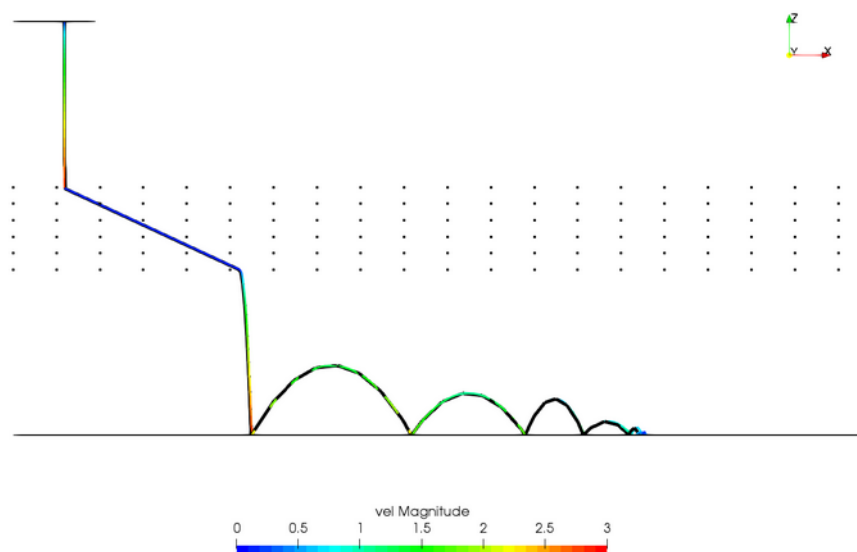
$$PAC = 100 \frac{\sum A_p}{A_{ele}}$$

PAC can then be converted to the corresponding cleanliness level given some slope  $C$ . Perry [13] provides a simple to use equation to map PAC to level. However, in experimenting with that model, we found the results to deviate by up to 5% for some values of  $C$ . Therefore, CTSP uses a lookup table to map PAC to level. The codes pre-computes the PAC for a range of levels and then uses linear interpolation to map the PAC to the level.

### III.d) Subcycling

Since version 1.0, the code supports particle push subcycling. In PIC or DSMC simulations, the time step is typically set based on volume cell size such that particles do not travel more than a cell per time step. This rule is not applicable to CTSP due to the mesh-free nature of the particle push. Therefore, the code attempts to find the correct time step automatically. The user provided time step is used to integrate position and velocity through a "full step". The code then performs the integration using a specified number of steps. With two steps, the integration is performed through two half time steps. The resulting position and velocity vectors are compared to each other and if within a given tolerance (30 degrees by default), the code uses the selected time step. Otherwise, the process repeats with  $0.5 \cdot dt$ . The process repeats until an optimal time step has been found. This is illustrated in Figure 5. The colored trace corresponds to a

simulation run with  $dt=0.1$  s, while the black trace is  $dt=1e-4$ s. Without subcycling, the 0.1s time step would produce an incorrect trace. With subcycling, both simulations produce an identical trace. Subcycling is turned on automatically for particulates but is disabled by default for molecules.



*Figure 12. Identical particle trace with 0.1 and 1e-4 s time step*

## IV. Examples

The code is shipped with a several examples, three of which are described in detail below. These examples correspond to the demonstration cases discussed in the 2018 J. Spacecraft and Rockets article[1], and as such, are found in the "JSR" folder. The first one verifies the molecular outgassing model by computing the steady-state distribution of a contaminant inside a closed vessel. The second example simulates a commonly encountered engineering task: using a quartz crystal microbalance (QCM) to characterize the outgassing rate of a test article exposed to vacuum. The final example demonstrates the use of gaseous purge to reduce infiltration of particulate contaminants.

### IV.a) Belljar

We start by considering a common task encountered by contamination engineers: using a QCM to determine the outgassing rate of some test article during a vacuum bakeout. The files for this example are located in **dat/belljar**. The geometry consists of a bell jar containing a platen supporting a harness (the test article), a scavenger plate, and a QCM. The bell jar is pumped by a cryopump connected by a long duct. The CAD drawing and the corresponding surface mesh are shown in Figure 13.

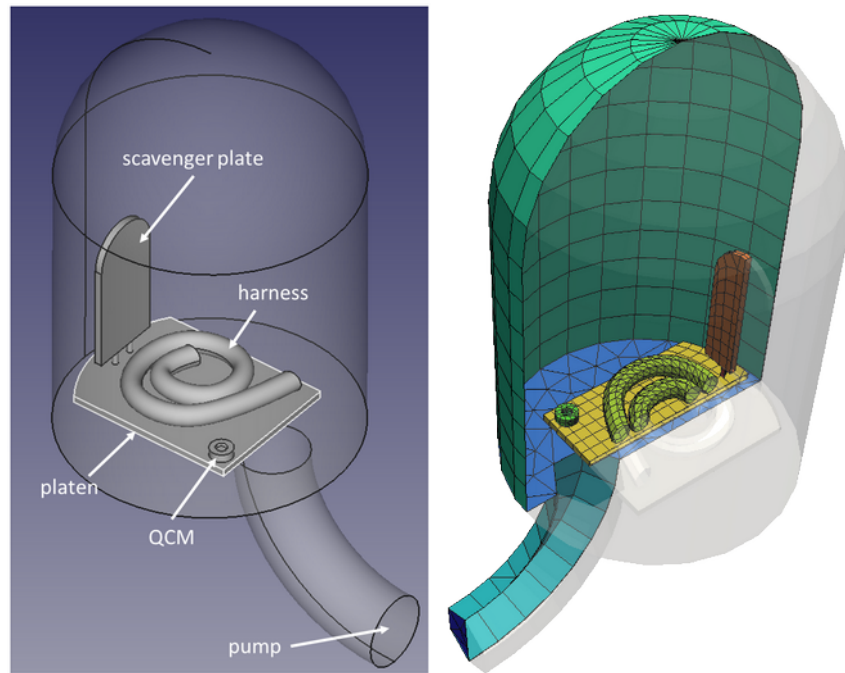


Figure 13. Geometry and the corresponding mesh for the belljar example

From mass conservation, we know that  $\Gamma_h A_h - \Gamma_q A_q - \Gamma_p A_p = 0$ , where  $\Gamma$  is flux and  $A$  is area, and the subscripts correspond to the harness, QCM, and the pump. For equally cold sinks,  $\Gamma_q = \Gamma_p$ . The mass balance equation can then be rewritten as  $\Gamma_h A_h k_{h \rightarrow q} = \Gamma_q A_q$  where

$$k_{h \rightarrow q} = \frac{A_q}{A_q + A_p}$$

is the view factor. In other words, knowing the view factor, we can relate the deposition rate on the QCM to the outgassing rate of the hardware (the harness). The difficulty arises in that we do not have a value for the effective pump area  $A_p$ . This value will always be smaller than the cross-sectional area of the physical pump since pump effectiveness will be reduced by the duct conductance, pumping speed inefficiencies, and so on. One way we can obtain this value experimentally is by introducing a secondary cold surface, such as a scavenger plate [8]. Figure 14 compares the sources and sinks in a vacuum chamber without and with a scavenger plate.



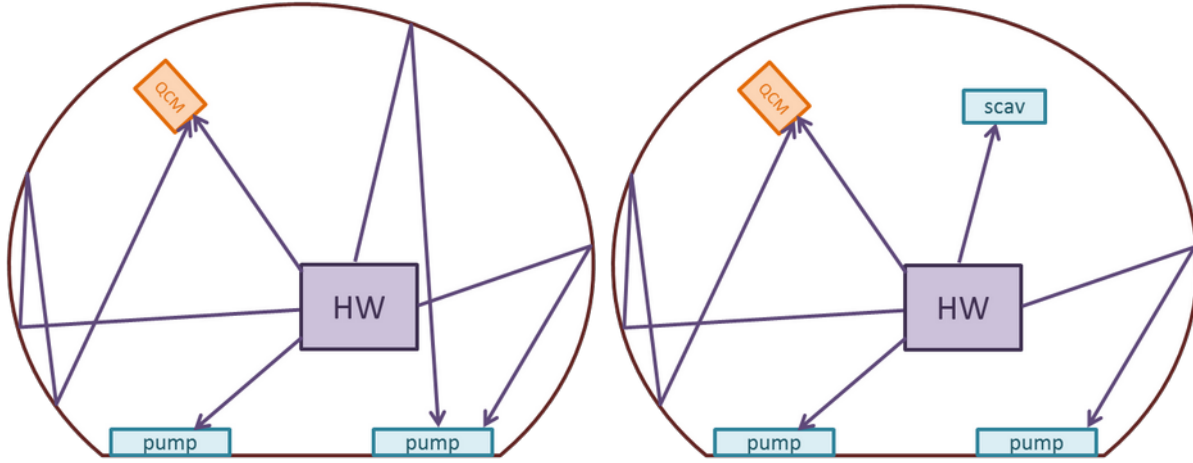


Figure 14. Chamber schematic without and with a scavenger plate

Again writing the mass conservation relationship for these two cases, we have

$$\Gamma_h A_h \left( \frac{A_q}{A_q + A_p} \right) = (\Gamma_q)_1 A_q \quad (\text{Ex-1})$$

$$\Gamma_h A_h \left( \frac{A_q}{A_q + A_p + A_s} \right) = (\Gamma_q)_2 A_q \quad (\text{Ex-2})$$

Where  $(\Gamma_q)_1$  and  $(\Gamma_q)_2$  are QCM fluxes without and with the scavenger plate. We now have two equations for two unknowns. Combining them, we obtain an expression for the effective pump area.

$$A_p = \frac{A_q [(\Gamma_q)_1 - (\Gamma_q)_2] + A_s (\Gamma_q)_2}{[(\Gamma_q)_1 - (\Gamma_q)_2]} \quad (\text{Ex-3})$$

Just as in an experiment, we start by collecting steady-state QCM flux with the scavenger at room temperature,  $(\Gamma_q)_2$ . We then numerically flood the scavenger by dropping its temperature to a cryogenic value cold enough to collect the contaminant. This will give us a value for  $(\Gamma_q)_2$ . Using combined areas of the QCM and scavenger mesh elements, we can then compute the effective pump area. Finally using this value we can numerically correlate  $\Gamma_q$  to  $\Gamma_h$ .

The simulation input file, **ctsp.in**, is listed below

```
#set some option
options{randomize:true, num_threads:4, log_level:info}

#load surface
surface_load_unv{file_name:"jar.unv"}
surface_load_unv{file_name:"harness.unv"}
surface_load_unv{file_name:"platen.unv"}
surface_load_unv{file_name:"scav-both.unv"}

#flush QCM with the platen otherwise particles get stuck in a 0.1mm gap
surface_transform{op:reset}
surface_load_unv{file_name:"qcm.unv"}
surface_transform{op:translate, offset:[0,0,-0.000095]}
surface_save_vtk{file_name:geom,format:ascii}

#specify volume mesh
volume_mesh{dx:0.01,dy:0.01,dz:0.01,expand:0.01}

#specify material properties
```

```

solid_mat{name:al, weight: 100}
molecular_mat{name:hcl, weight: 94, mpw: 2e10, r:1.55e-10}
molecular_mat{name:n2, weight: 28, mpw: 5e14, r:1.55e-10}

#set material interactions
material_interaction{source:hcl, Ea_des:12, C_pow:1}
material_interaction{source:n2, Ea_des:3.5, C_pow:0.01}

#specify component data, scavenger transition to 100K at t=10s
surface_props{comps:./, mat:al, temp:350, c_outgas:0.0}
surface_props{comps:scav, mat:al, temp:[350@0,350@1,0@1.0001]}
surface_props{comps:pump, mat:al, temp:0}
surface_props{comps:qcm, mat:al, temp:0}
surface_props{comps:harness, mat:al, temp:350}

#example of setting initial molecular loading, although we use cosine source instead
#load_molecules{comps:harness, trapped_mats:[1.0*hcl], trapped_mass:0, surf_mats:hcl,
surf_height:0}
#source_outgassing{model:pow}

#set contaminant injection settings
source_cosine{comps:harness, mass_flux:1e-8, mats:[1.0*hcl], v_drift: 100}

#save animation data
particle_trace{file_name:trace,mat:hcl,ids:3}
surface_save_vtk{skip:200,file_name:"surf",vars:[surf_height.hcl, temperature]}
volume_save_vtk{skip:200,file_name:"field",vars:[pressure,nd.hcl,t.hcl,u.hcl]}

#save restart data every 5000 time steps
restart_save{skip:5000}

#run simulation of 2s of real time, show/save log every 5 time steps
run_sim{dt:2e-4,num_ts:10000, log_skip:5}

```

For this particular example, the surface mesh was split into multiple files: *jar.unv*, *harness.unv*, *platen.unv*, *scav.unv*, and *qcm.unv*. We load these surfaces using **surface\_load\_unv**. While loading the QCM geometry, we also translate the QCM slightly in the  $-z$  direction using **surface\_transform{op:reset}** and **surface\_transform{op:translate}**. This translation is needed since the QCM, as loaded, is not perfectly flushed with the platen but instead there is a tiny ( $<0.1\text{mm}$ ) gap separating the two. During the simulation, some particles would eventually reach this gap. These particles continue bouncing between the platen and the bottom of the QCM, noticeably slowing down the simulation as many surface hits need to be checked during a single time step. Next a volume mesh is created using **volume\_mesh**. We will use the mesh to compute bulk gas properties such as density and pressure. Materials are specified next using **solid\_mat** and **gas\_mat**. The latter command generates some hypothetical 94 AMU hydrocarbon with activation energy 12 kJ/mol used on impact with all materials. This value of  $E_a$  will prevent the molecule from sticking at room temperature surfaces. The specific weight is set to  $5e13$  real molecules per simulation particle. Higher value will result in the simulation running faster at the expense of noisier results.

Base materials and surface temperatures are then assigned to surface components using **surface\_props**. The first command uses a regular expression to assign default values to all surfaces. Specifically of interest is that surface temperature is set to 300K. The pump and QCM crystal are assigned cryogenic temperatures. The pump is set to 15K while the QCM is set to 100K. This difference has no impact on this particular setup since our example hydrocarbon sticks equally well to both surfaces. The difference may be important if we were interested in including lighter gases like nitrogen, in which case the higher QCM crystal temperature could be used to selectively avoid deposition of that gas. A list of tuples is used to set temperature on the scavenger. The property *temp:[300@0,300@10,100@10.5]* will set the scavenger temperature to 300K at  $t=0\text{s}$ . CTSP linearly interpolates between the provided data, and hence temperature will remain 300K until  $t=10\text{s}$ . It will then rapidly drop to 100K at  $t=10.5\text{s}$ . The scavenger will then remain at this final temperature until the simulation finishes.

All components by default contain zero trapped mass and zero mass flux. We could next assign some trapped mass to the *harness*, but instead of doing that, we instead prescribe a constant  $1\text{e-}8\text{ kg/m}^2/\text{s}$  constant mass flux out of all surface elements on this component with the help of **source\_cosine**. The outgassed material will consist of 100% “hc1” molecules. We next enable periodic saving of surface and volume files using **surface\_save\_vtk** and **volume\_save\_vtk**. For now, it is not necessary to specify list of variables to save on the surface as the code saves all available data. Variables need to be specified for the volume mesh, however. We specify to output total pressure, and number density and temperature of the “hc1” gas material. Data will be saved every 10000 time steps, with data averaged between the saves.

This simulation may take about an hour to complete. Figure 15 shows the progression of surface contaminant thickness and the hydrocarbon gas number density visualized in Paraview. The first plot corresponds to a time shortly after the simulation starts. We can notice that all surfaces are colored white, indicating no hydrocarbon deposition, with the exception of the QCM crystal and the pump. The second plot shows the chamber just prior to the scavenger activation. The contaminant number density has increased and so has the deposition thickness on the QCM and the pump. All other surfaces still show no deposition. The third plot shows the state as the scavenger starts transitioning cold. We can immediately note the decrease in the contaminant number density (which corresponds to a decreased chamber pressure) as well as the presence of the contaminant on the scavenger plate. The final picture shows the chamber at an even latter time. The contaminant thickness on the scavenger has increased and the chamber pressure has dropped even further.

At a 5 time step interval, CTSP saves time dependent global data to **ctsp\_diag.csv**. A snippet is below.

```
it,time,np.HCl,real.HCl,trapped_mass.JAR,surf_h.JAR,trapped_mass.JAR_BASE,surf_h.JAR_BASE,
E,trapped_mass.JAR_HOSE,surf_h.JAR_HOSE,...
0,0,0,0,0,0,0,0,0,0,0,0,0,1,0,0,0,0,0,0,0,0,0,0,0,0,0
5,6.944444e-007,0,0,0,0,0,0,0,0,0,0,0,1,0,0,0,0,0,0,0,0,0,0,0
```

The fields include the current time step, current time, the number of simulation and real molecules, as well as the total mass of a molecular contaminant on each component. We can then plot the “trapped\_mass.QCM” column against the time step “it” to generate a plot as shown in Figure 16. We can clearly see three different regimes. First, between time step 0 and 20000, the deposited mass grows in a non-linear fashion. Subsequently, growth reaches constant rate. This second region corresponds to the steady state with the scavenger turned off. The slope,  $\dot{m}_q$ , can be converted to flux using  $(\Gamma_q)_1 = (\dot{m}_q)_1/A_q$ . We obtain  $A_q$ , the total surface area of QCM crystal mesh elements by reviewing **ctsp.log**:

OCM (8), area: 1.107917e-004

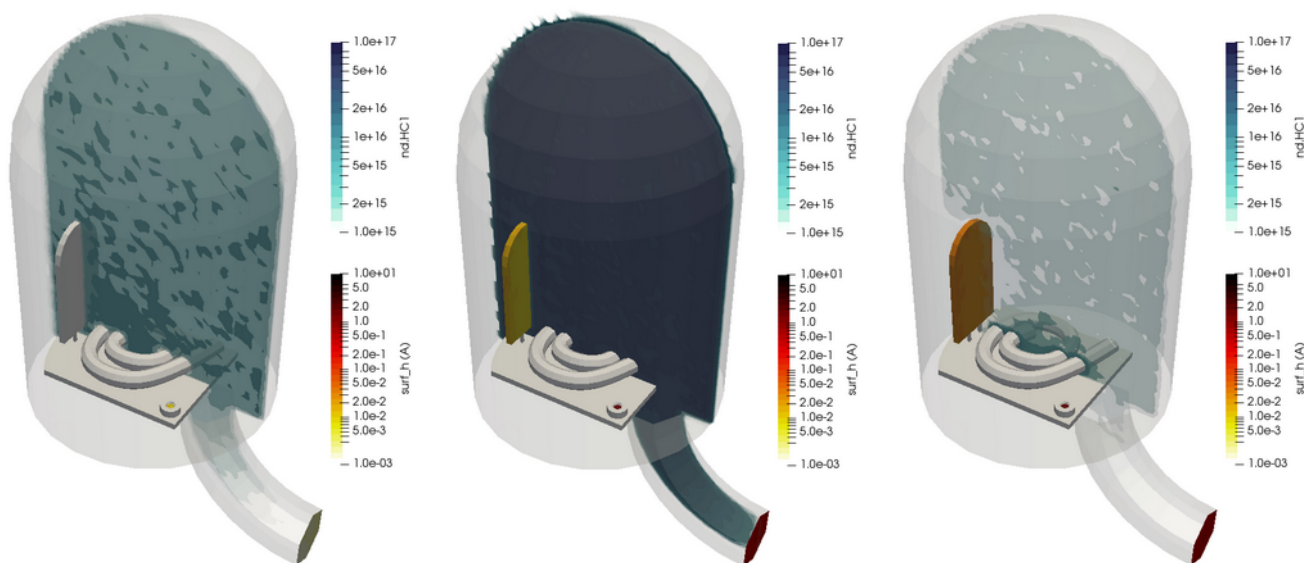


Figure 15. Hydrocarbon density and surface layer height shortly after simulation starts, right after scavenger activation, and at a later time.

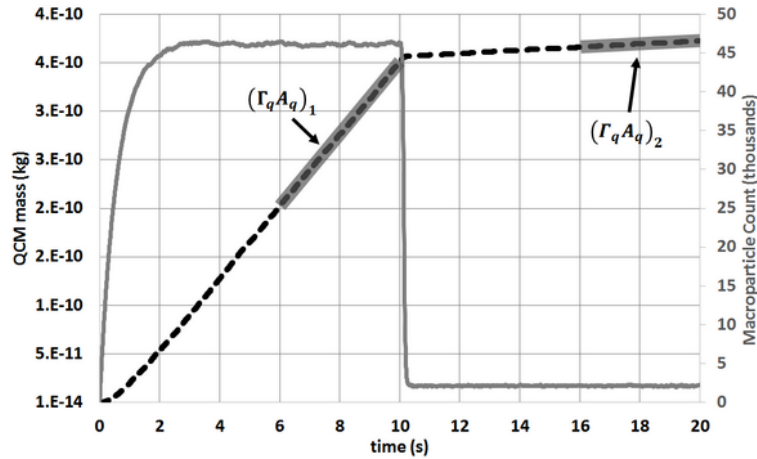


Figure 16. QCM deposited mass versus time step

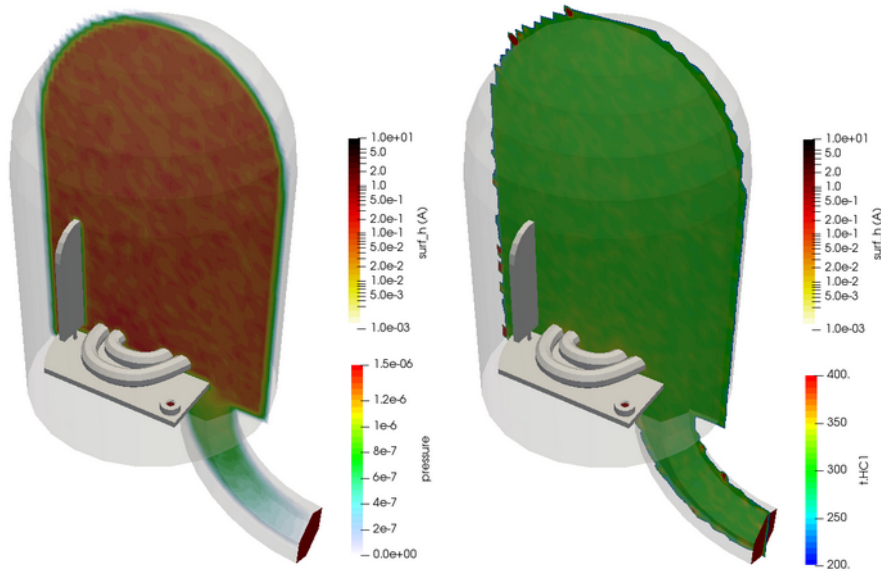


Figure 17. Pressure and temperature just prior to scavenger activation

By comparing the slopes with and without the scavenger, the effective pump area is found to be over 4x smaller than the geometrical pump cross-section due to conductance loss in the duct. We find the harness outgassing rate to be  $1.03\text{e-}8$  kg/s, about 2.6% higher than the expected value. Although ideally we would expect this error to be zero, this agreement is still excellent. Figure 17 visualizes the other saved volume properties: pressure and temperature. Pressure is obtained from  $P = nkT$ . As expected, gas temperature is uniform and equal to the surface 300K temperature.

#### IV.b) Molecular Equilibrium

Consider a solid sphere placed inside a larger, hollow sphere. This closed system can be used to test various aspects of the molecular transport model. We let the inner sphere initially contain some molecular contaminant trapped within it but the rest of the system is initially contaminant free. Clearly, this system is not at equilibrium. The molecules present inside the sphere (region I) are expected to diffuse to the surface (region II) and then desorb into the gas phase (region III). These molecules will then impact the outer sphere and some fraction will deposit onto the outer sphere surface (region IV). These molecules then diffuse into the outer sphere bulk material (region V). At steady-state, concentration gradients between these five regions must vanish. For instance, we have

$$-\frac{dn_c}{dt} \equiv H(n_c, \theta) = n_c - \gamma\theta$$

so that at steady state  $N_c = \gamma\theta$ . We define  $n_c = N_1/V_i$ , where  $N_1$  is the number of molecules inside the inner sphere with volume  $V_i$ . Similarly,  $\theta = N_2/A_i$ , with  $N_2$  being the number of molecules in the surface layer and  $A_i$  is the surface

area of the inner sphere. The equilibrium partition coefficient is set to  $\gamma = 1 \text{ m}^{-1}$ . Furthermore the adsorption and desorption fluxes must also be equal,  $\Gamma_a = \Gamma_d$ . From kinetic theory, the adsorption flux is given by  $\Gamma_a = (N_g \bar{u}) / (4V_g)$  where  $N_g$  is the number of molecules in the gas phase and the mean velocity  $\bar{u} = \sqrt{8kT/\pi m}$ . The volume occupied by the gas is given by  $V_g = (4/3)\pi(r_2^3 - r_1^3)$ . The desorption flux is  $\Gamma_d = \theta/\tau_r$ . Here we ignore any multilayer effects. At steady state we thus require

$$\theta = \left( \frac{\bar{u}\tau_r}{4V_g} \right) N_g \equiv k_g N_g$$

We run this model for two temperature configurations. The first assumes that the entire system is isothermal with both spheres at  $T=250 \text{ K}$ . The radius of the inner sphere is  $r_1 = 10 \text{ cm}$ . The outer sphere has inner radius  $r_2 = 1 \text{ m}$  and is assumed to be  $1 \text{ cm}$  thick. The inner sphere contains  $10^{-10} \text{ kg}$  of some hypothetical contaminant with  $m_a = 94 \text{ amu}$ ,  $(E_a)_{dif,des} = 12 \text{ kcal/mol}$ , and  $r = 1.5 \times 10^{-10} \text{ m}$ . The diffusion coefficient is  $D = 20 \text{ m}^2/\text{s}$ . The exact mass generation model generating particles with fractional weight is used. The simulation was run for  $10,000 \Delta t = 10^{-4} \text{ s}$  time steps. Figure 18 shows the evolution of  $n_c, \theta, k_g N_g, \theta_2$  and  $n_{c,2}$  versus the simulation time step. The system reaches equilibrium around time step 6,000 with all concentration gradients vanishing. This figure also shows the corresponding combined mass of molecules in each of the five zones. We can see that the total mass remains constant. Figure 19 plots the typical contaminant partial pressure in the cavity between the spheres. This is an example of a macroscopic data that can be computed due to CTSP concurrently pushing multiple particles. Pressure was computed by scattering particle positions to a Cartesian mesh to compute number density  $n$ . Temperature is also computed from particle velocities. Pressure can then be obtained from the ideal gas law. This figure also plots the surface concentration in the number of particles per unit area. The average of these element values is represented by the dashed lines in Figure 18. The increased noise on the inner sphere is due to the smaller surface elements.

We next consider a case with the outer sphere temperature reduced to  $200 \text{ K}$ . This result is plotted in Figure 20. Now the bulk and surface layer regions form an internal balance but there is no longer an equilibrium between the small and the large sphere. This is expected. Since the larger sphere is colder, we expect it to act as a better sink for the contaminants. The molecular concentration should thus be higher on the outer sphere, which is indeed confirmed by the simulation. The gas phase concentration now also tracks the larger  $200 \text{ K}$  sphere.

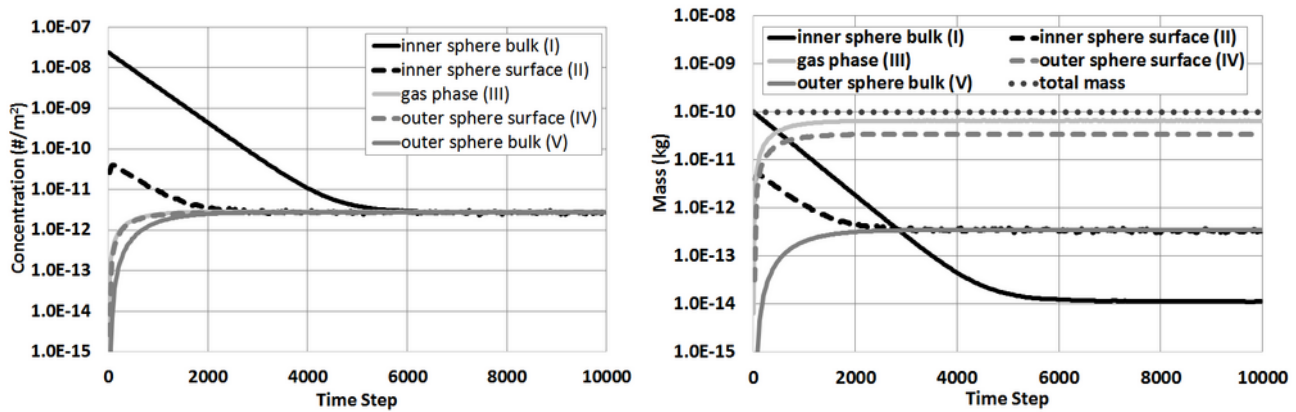


Figure 18. Molecular concentration and molecular mass for the isothermal spheres case

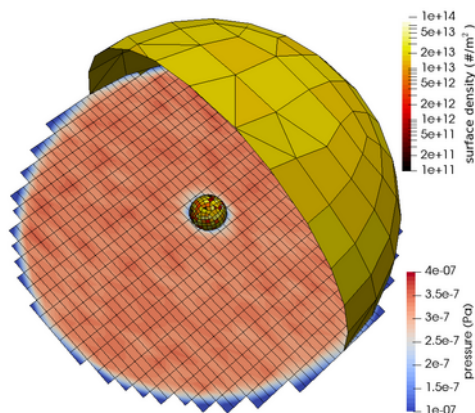


Figure 19. Typical pressure and surface density for the isothermal case

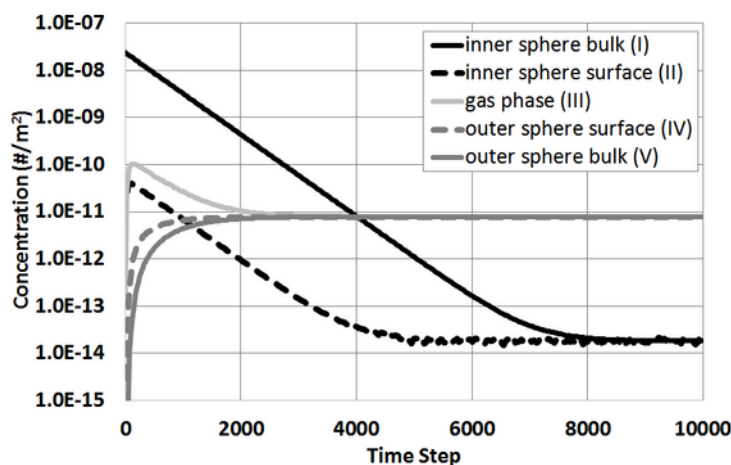


Figure 20. Evolution of molecular concentration with 200K outer sphere. Gas phase concentration computed using  $T = 200$  K.

The input file for this case (in `dat/spheres`) is listed below. The input geometry file, `spheres.unv`, contains the two spheres with normal vectors facing into the gas cavity, and zone names set as "inner" and "outer".

```
#set options
options {log_level:info, domain_check:true, randomize:false, num_threads:1, screen_diag_freq:25,
file_diag_freq:2}

#load surface
surface_load_unv{file_name:"spheres.unv"}
surface_save_vtk{file_name:"surf-all"}

#define volume mesh
volume_mesh{dx:0.04,dy:0.08,dz:0.08, expand:0.02}

#define materials and material interactions
solid_mat{name:metal, weight: 100}
molecular_mat{name:hcl, weight: 94, mpw: 1e10, r:1.55e-10}
material_interaction{source:hcl, target:*, Ea_des:12, C_dif:2.5e11}

#define inner and outer sphere properties
surface_props{comps:inner, mats:metal, volume: 4.189e-3, temp:250 }
```



```

surface_props{comps:outer, mats:metal, volume: 1.269e-1, temp:250}

#enable outgassing
load_molecules{comps:inner, trapped_mass:1e-10, trapped_mats:[1.0*hc1]}
source_outgassing{model:fang, stop_it:-1, exact:true}

#set output
particle_trace{file_name:trace,mat:hc1,num_traces:20, skip:100}
volume_save_vtk{skip:1000,file_name:"field",vars:[nd.hc1,t.hc1]}
surface_save_vtk{skip:1000,file_name:"surf",vars:[surf_h.hc1,dep_rate.hc1,T]}

#run simulation
run_sim{dt:1e-4,num_ts:2000,diag_start:0,diag_skip:5}

```

#### IV.c) Particulate Transport

In this example we consider the effect of nitrogen purge on particulate contamination. Suppose that some instrument containing two detectors is stored on a lab bench. The instrument is connected to a nitrogen purge which vents out around the perimeter of the larger of the two detectors. An impact to the bench dislodges particles from a shelf located above the detector. We are interested in numerically studying the effectiveness of the purge on preventing contamination of the detector. The entire set up can be seen in Figure 21. The mesh shown in the second image correspond to five different zones. Note that only the bottom surface of the top shelf is modeled. The normal vectors are oriented to point away from the solid surface into the simulation volume. Files for this example are in **dat/purge**.

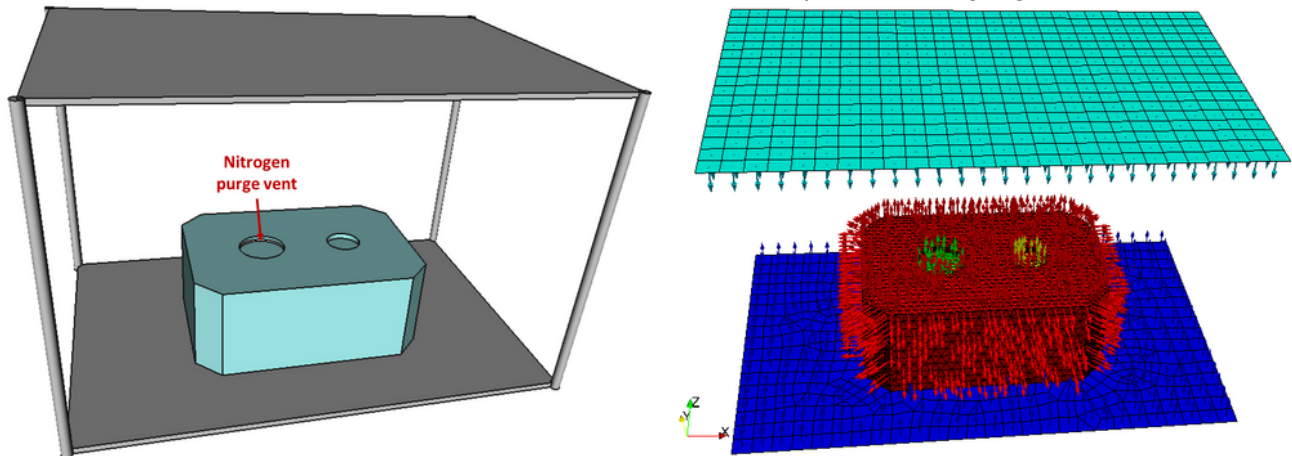


Figure 21. Geometry model and the corresponding mesh for the purge example.

The simulation input file, `ctsp.in` is listed below:

```

options{randomize:false, num_threads:1}

#set ambient environment
world{gravity:[0,0,-9.81], pressure:101325, temperature:300}

#load surface
surface_load_unv{file_name:"surf-mesh.unv",units:m}

#volume mesh added to remove particles leaving the domain
volume_mesh{dx:0.1,dy:0.1,dz:0.1}

#component information, setting coefficient of restitution to 0.5
surface_props{comps:./, mat:al, temp:0,c_rest:0.5}

#load cfd data, comment out to use still air at constant pressure per world
flow_load_csv{file_name:"purge_1e-3.csv", map_pos:[4,5,6], map_vel:[0,1,2], time:-1, save_view:
false}

```

```
#specify materials
solid_mat{name:al, weight: 100}
particulate_mat{name:flakes, density:2700, integrator:subcycle}

#load level 600, slope=0.926 particulates, model detachment with Klavins-Lee 4g acceleration
load_particulates_1246{comps:top, mat:flakes, particle_count:200000, level:600, C:0.926}
detach_particulates{model:klavins, klavins_accel_mag: 39.24, release_interval:-1}

#setup particle trace and periodic particle saving for animations
particle_trace{file_name:trace,mat:flakes,num_traces:100}
particle_save_vtk{file_name:"particles", mat:flakes,skip:25, num_particles:2000,max_id:300000}

#save animation of surface composition
surface_save_vtk{skip:25,file_name:"surf",vars:[level,pac]}

#enable histogram output
surface_save_histogram{file_name:"hist",skip:100,                                     bins:
[1,10,20,30,40,50,60,70,80,90,100,200,300,400,500,600,700,800,900,1000]}

#run simulation
run_sim{dt:0.001,num_ts:4000,diag_start:1,diag_skip:100}

#save final surface data
surface_save_vtk{file_name:"surf-final",vars:[level,pac]}
```

We first set ambient environment using **world**. Specifically, we let gravity act in the  $-z$  direction, and prescribe 1 atm background pressure. Next, we use **surface\_load\_unv** to load the surface mesh from the surf-mesh.unv file. We specify that dimensions are in meters, which is also the default. Next a volume mesh is created using **volume\_mesh**. This mesh is being used delete particles leaving the volume mesh bounding box. This is important for computational reason since there are no surfaces in the  $\pm X$  and  $Y$  directions to stop particles. As will be apparent later, as the purge flow is increased, flow with non-negligible tangential velocity develops along the bottom of the top shelf. This flow acts to push particles laterally, and without the volume mesh, these particles would then fly out of the computational domain. Eventually gravity will make them travel in the  $-Z$  direction, but by then there will not be any floor present to stop them and these particles would continue traveling forever. Next we specify the coefficient of restitution using **surface\_props**. The same coefficient is assigned to all surfaces.

Next we load the flow data from a file using **flow\_load\_csv**. This command can be commented out to simulate particles settling out in a still air. The CFD solutions for this example were generated using OpenFoam. Simulation results were save in VTK format and were then saved as CSV in Paraview. The structure of the file is as follows:

```
"U:0","U:1","U:2","p","Points:0","Points:1","Points:2"
4.846505e-003,0.000000e+000,1.140431e-004,-1.259318e-004,-2.100000e-001,0.0e+00,0.0e+00
3.844443e-003,0.000000e+000,1.380693e-004,-3.659827e-004,-2.024971e-001,0.0e+00,0.0e+00
3.828275e-003,0.000000e+000,1.411461e-004,-7.318797e-004,-1.949940e-001,0.0e+00,0.0e+00
```

This file contains a point cloud of flow velocities and pressures. As can be seen, the three velocity components are stored in columns [0,1,2], while positions are in [4,5,6]. Relative pressure is in column 3. Since the deviations in pressure are so small, we ignore this column (there is no **map\_pressure**) specified, and instead the code will utilize the constant value from **world**. The *time:-1* field tells CTSP to use this file for the entirety of the simulation.

The simulation next specifies material properties using **solid\_mat** and **particulate\_mat**. We use the latter command to specify density (which is used to compute mass) of the particulate “flakes” coming off the top shelf. The actual distribution of these is specified by the **load\_particulates\_1246** command. We tell the code that we would like to generate level 600 and slope 0.926 distribution of particulates on component “top”. We use the Klavins and Lee release model with release acceleration equal to 4g via **detach\_particulates**. The particles should be all released at once at the first time step, as noted by *release\_interval:-1*.

Next we enable tracing of particles with **particle\_trace**. We tell the code to generate traces for random 100 “flakes” particles in the id range of [0,100000]. We also let the code save the positions of 2000 particles every 10 time steps with



**particle\_save\_vtk.** This command will save positions of the same particles (as opposed to sampling random particles at each save) so it can be used to generate animations. We also enable a surface composition histogram output with **surface\_save\_histogram.** We are then ready start the simulation using the **run\_sim** command. We tell the code to run for 10000 time steps. Volume diagnostics are computed once every 100 steps. Since we are not interested in the any of these data, this interval could be set even higher. Once the simulation finishes, surface results are saved with **surface\_save\_vtk.** Note that here we use a `vars:[level,pac]` which is currently ignored but may be added in the future. For now, this command saves all available surface properties.

Figure 22 shows typical results from the simulation for static air (no flow), and Figure 23 shows results for purge flow at  $1\text{e-}4$ ,  $2\text{e-}4$ ,  $5\text{e-}4$ , and  $1\text{e-}3$   $\text{m}^3/\text{s}$ , respectively, visualized using Paraview. These results were obtained by running the CTSP 5 times with different file specified for the **flow\_load\_csv** command. The no flow case was obtained by commenting out this command entirely. Since only the bottom surface of the top shelf was included in the mesh, the coloring we see in the plot actually corresponds to the PAC on the downward facing surface. As can be noted, the magnitude of PAC is approximately constant for the entire source surface. This is indeed the value that we obtain. Similarly an approximately constant value is obtained on all upward facing surfaces, despite differences in mesh density. This indicates that the result is not mesh dependent. We can numerically compute (see `drag.py`) the expected PAC on the top shelf after particle detachment to find that it should equal to 0.351427. The small variations in value from cell to cell are due to the statistical nature of the simulation. Rerunning the simulation will result in a slightly different variation, which could be averaged as part of post processing to further reduce the noise. The level of noise also decreases with an increase in the number of particles per bin given by the `parts_per_bin` parameter.

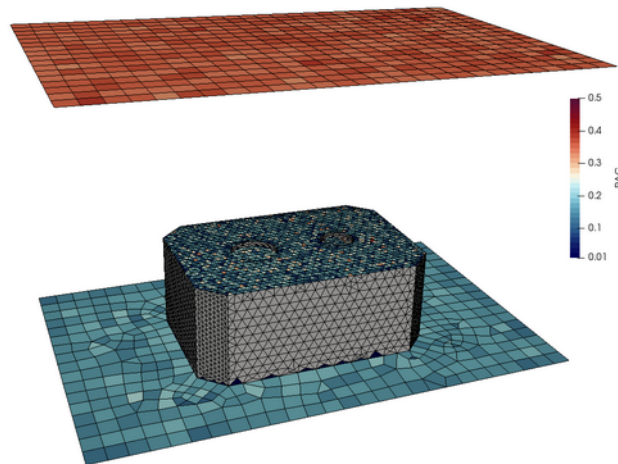


Figure 22. Simulation results showing the surface particle area coverage for no flow.

Figure 24 shows the top down view of the instrument. As the purge flow rate is increased the PAC on the detector is reduced. At  $1\text{e-}4$   $\text{m}^3/\text{s}$ , the reduction is mainly limited to a circumferential strip around the vent inlet. This region grows with increasing flow rate. At  $1\text{e-}3$   $\text{m}^3/\text{s}$ , the purge flow rate is sufficiently strong to generate an “umbrella” over a large portion of the instrument, effectively shielding not only the larger detector, but also the smaller one that does not have an associated flow.

To further analyze the effect of purge flow, we may be interested in determining the average PAC on the detector for each flow rate. This could be done in Paraview by selecting mesh elements on the detector and using the Integrate filter. However, CTSP already prints this information to the **ctsp.log** file. Below is the example output. For each zone, the particulate PAC as well as particulate level, assuming  $C=0.926$ , is printed.

FLOOR:	0.000e+000 (A, surf_h)	1.396e-001 (% , PAC)	4.607e+002 (level)
TOP:	0.000e+000 (A, surf_h)	3.514e-001 (% , PAC)	5.562e+002 (level)
DET1:	0.000e+000 (A, surf_h)	7.120e-003 (% , PAC)	2.063e+002 (level)
DET2:	0.000e+000 (A, surf_h)	1.576e-001 (% , PAC)	4.670e+002 (level)
UNNASIGNED:	0.000e+000 (A, surf_h)	3.427e-002 (% , PAC)	1.466e+002 (level)

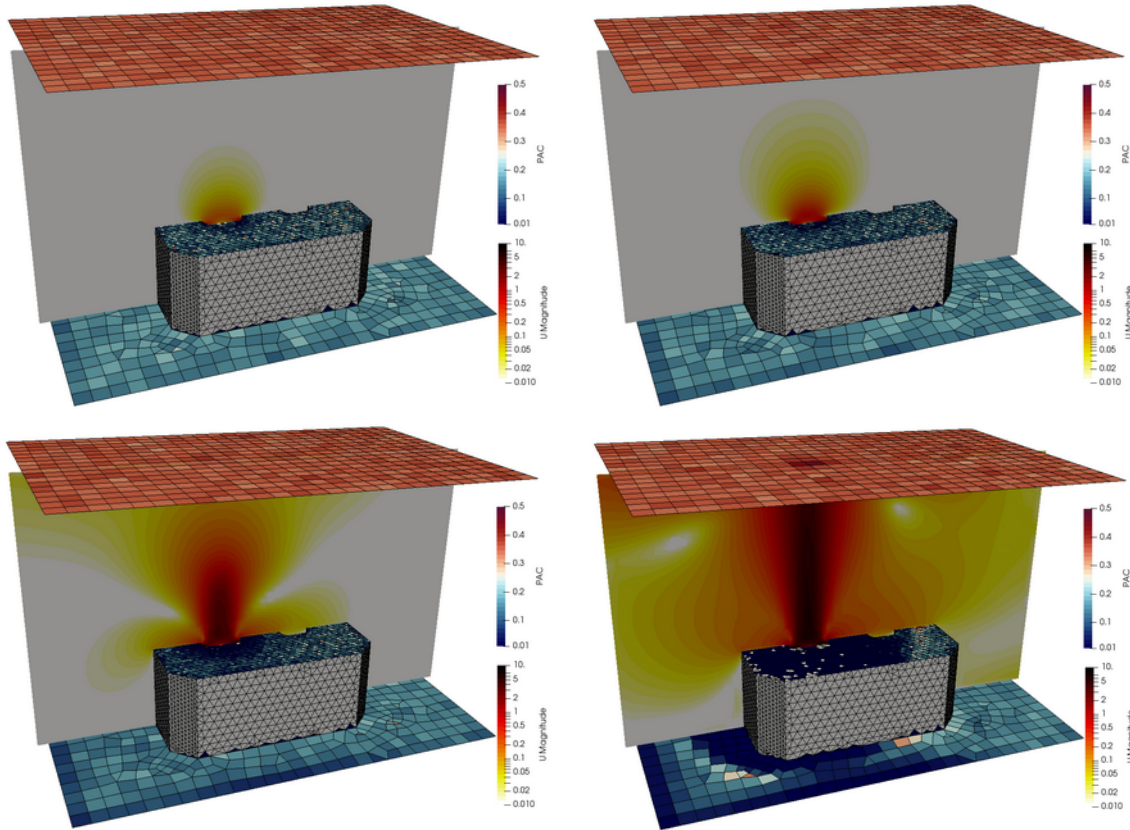


Figure 23. Simulation results showing the surface particle area coverage as well as the corresponding velocity field for  $1\text{e-}4$ ,  $2\text{e-}4$ ,  $5\text{e-}4$ , and  $1\text{e-}3$   $\text{m}^3/\text{s}$ , respectively.

By capturing this data for the 5 cases, we can generate a plot shown in Figure 25. The solid line is the averaged simulation PAC on the larger detector as a function of purge flow rate. We can use this data for validation. The data shown by the dashed line was obtained by running a Python script **drag.py**. This script computes the number of particles in each 1Cm bin in [1,1000] and determines the fraction that is released according to the Klavins and Lee model at a prescribed *a\_mag*. It then computes particle areas and masses using the same algorithm utilized within CTSP, based on aspect ratios per a paper of Perry. In each bin, the code then balances the gravitation force versus drag force assuming a stationary particle and some prescribed uniform vertical velocity. If the drag force dominates, the particle is assumed not to be able to reach the detector. The cross-sectional areas of the remaining particles is summed up to obtain the effective PAC on the target. We can see a generally good agreement.

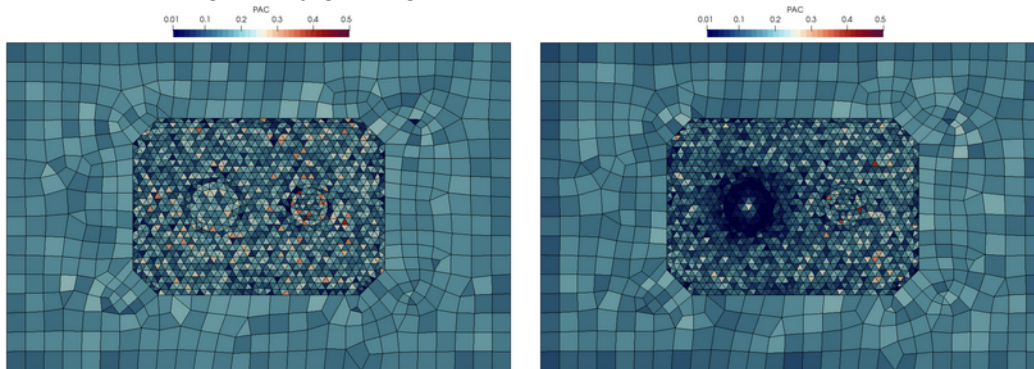


Figure 24. Top down view of the instrument for 0 and  $2\text{e-}4$   $\text{m}^3/\text{s}$  flow rate

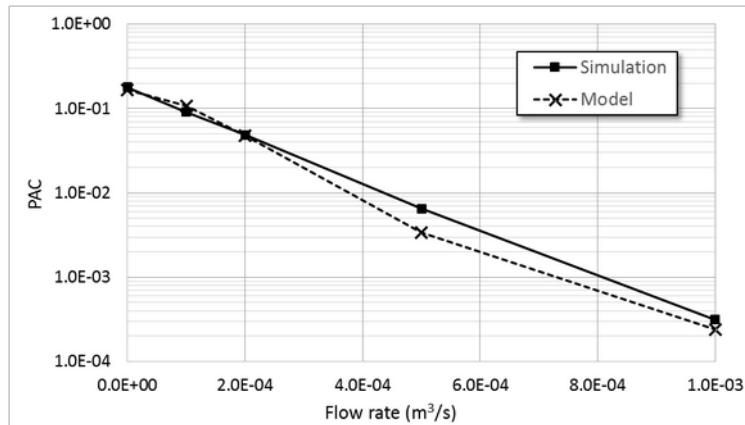


Figure 25. Comparison of simulation to model PAC

A major source of error in our simple Python model is that it assumes uniform flow velocity. But as can be seen from plots in Figure 23, the velocity field is highly non-uniform. The approach used to obtain representative velocity for the model was to select a large number of points near the detector, and use Paraview's histogram feature to obtain the average velocity magnitude (this approach was used since it appears that Paraview lacks a built in filter to average point data). The same data points were used across the 4 input files to maintain consistency.

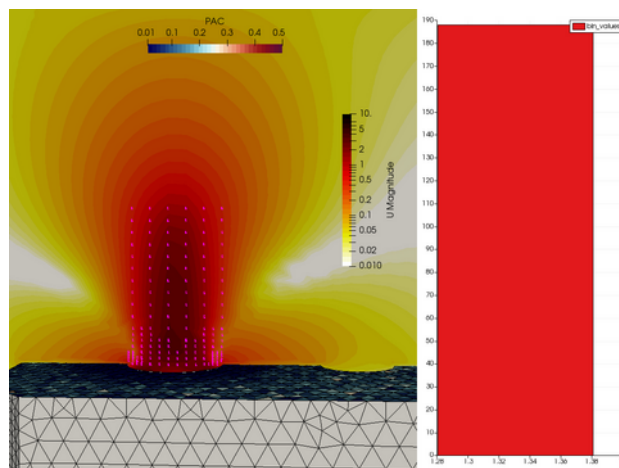


Figure 26. Data points used to sample flow velocity

Upon a closer inspection of plots in Figure 24, we may notice that the center of the detector appears to have higher particle deposition values than the surrounding areas. We can take a look at the generated traces in **trace.vtp** to better understand this issue. Figure 27 shows a typical result for the 5e-4 m³/s flow rate. Note that the CFD solution indicates that the highest velocity magnitude occurs some short distance above the detector and that there is actually a local minimum along the centroid. This seems to imply presence of a recirculating region. As shown by the trace, at the default coefficient of restitution of 0.5 particles bounce around quite a bit. As such it appears that some of these bounces bring particles onto the detector where they are constrained by this near-surface flow. The particles will naturally settle out at the local minimum. The result shown in the second image was obtained by reducing to 0.3. Particles are now less bouncy and the peak value on the detector is reduced (the triangle went from red to light blue). However outside this region the two solutions comparable.

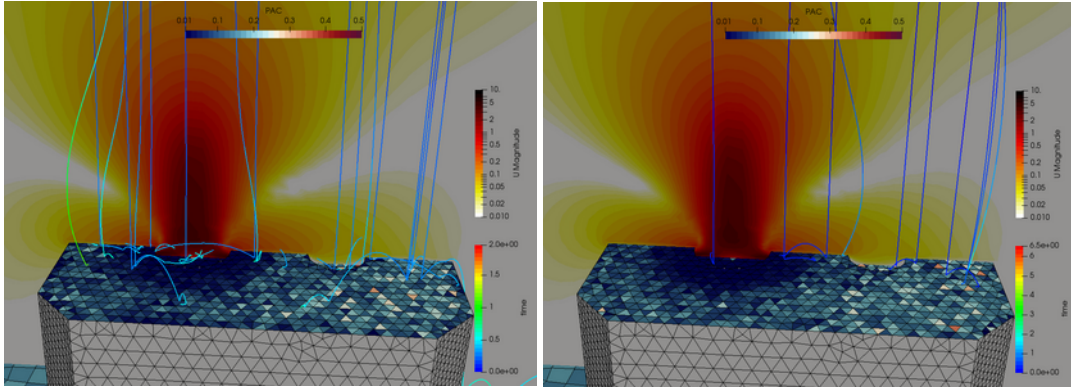


Figure 27. Particle traces with  $\alpha_{COR}=0.5$  on left and  $\alpha_{COR}=0.3$  on right

Finally, Figure 28 illustrates the ability to generate animations by visualizing data saved by **particle\_save\_vtk**. The **particles\_\*.vtp** files were loaded into Paraview and visualized using the glyph filter. Particles are colored according to their mass. We can see that the heavier (dark red) particles settle out first. The lighter (white) particles tend to remain suspended for a long time after the heavier particles have settled out.

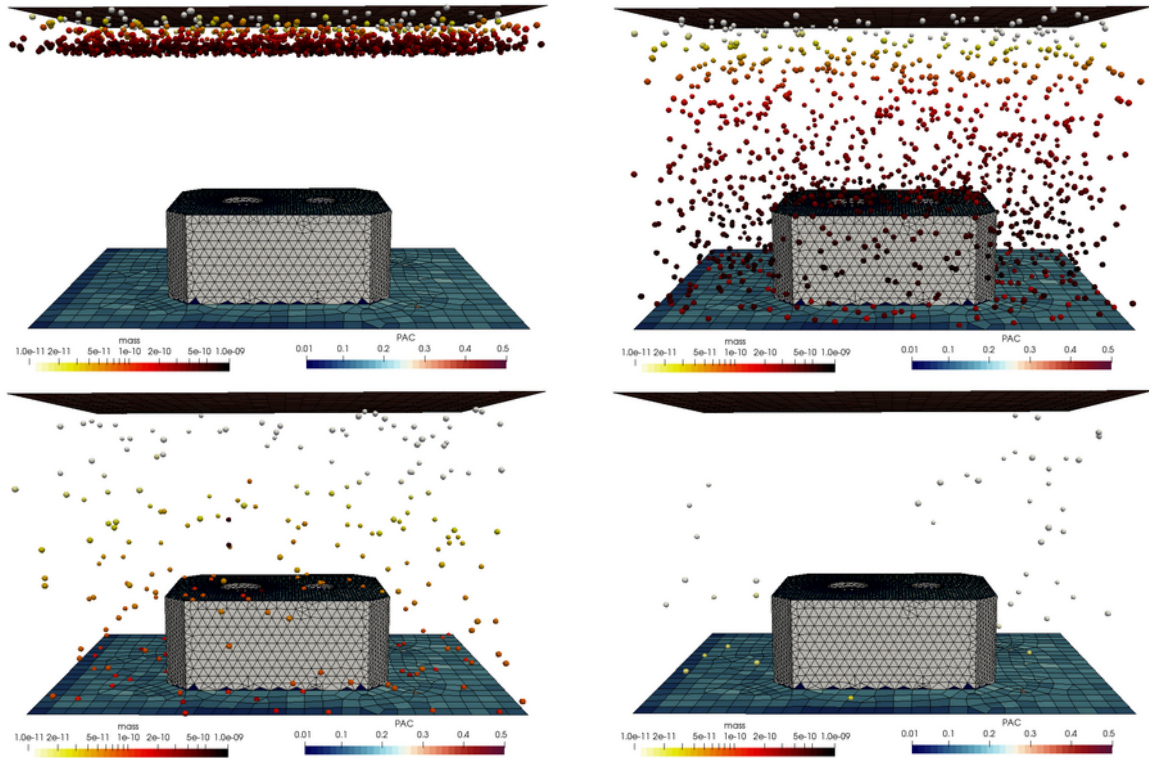


Figure 28. Heavier particles (red) settle out much faster than lighter ones (white).

#### IV.d) Additional Examples

The "dat" folder contains input files for several additional examples, which are summarized below.



#### IV.d.1) DSMC

The **DSMC** folder contains several examples of setting up a DSMC simulation. The "nozzle" subdirectory contains inputs for simulating flow through a converging nozzle. The "mesh-refine" directory illustrates how to set up a case with mesh refinement. Note that once the mesh is refined, VOLUME\_SAVE\_VTK will generate an unstructured mesh.

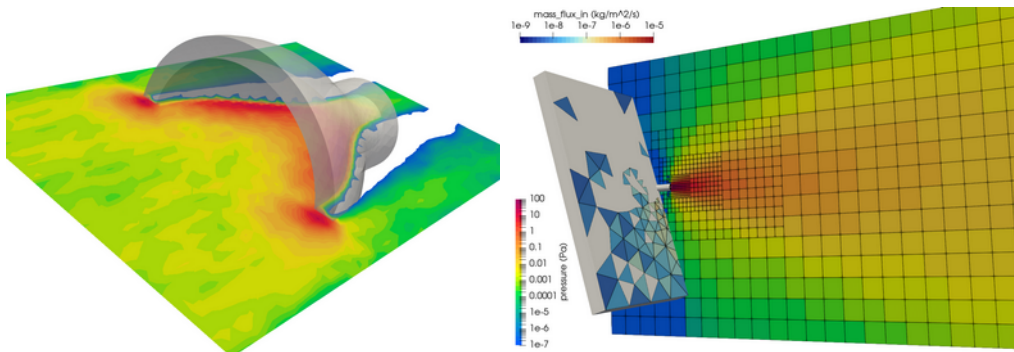


Figure 29. DSMC examples: flow through a nozzle, and plume expansion with mesh refinement.

#### IV.d.2) Molecules

Here you will find examples dealing with molecular transport. The **tube** folder contains inputs for simulating conductance through a cylindrical tube. This was the first-ever test of CTSP, but has not been verified in a while, so it may not be working properly anymore.

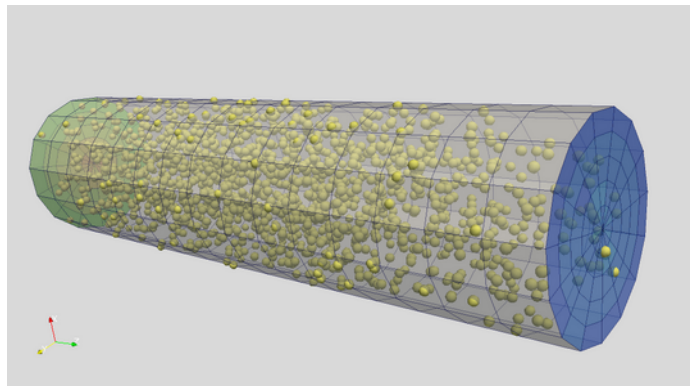
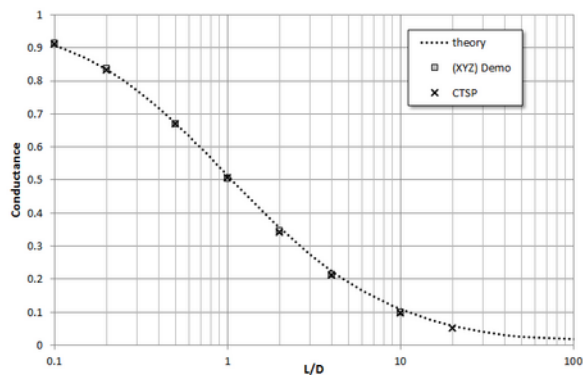


Figure 30. Simulation of conductance through a cylindrical tube

#### IV.d.3) Particulates

This folder contains example of particulate transport simulations. The **funnel** folder demonstrates how to simulate an ISO-14644-1 source to inject particulates above a funnel leading onto a floor which is initialized with an IEST-STD-1246 particulate population.

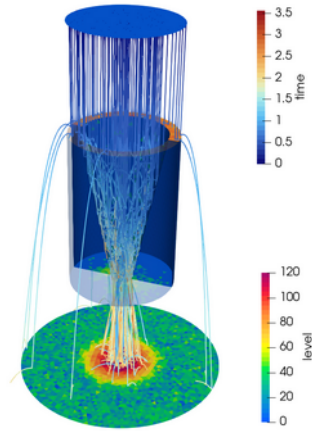


Figure 31. Traces of particulates and the corresponding cleanliness level

#### IV.d.1) Dynamics

The **dynamics** folder illustrates the use of surface translation. Right now it is possible to specify linear velocity, but rotation and momentum transfer from plume is still a work in progress.

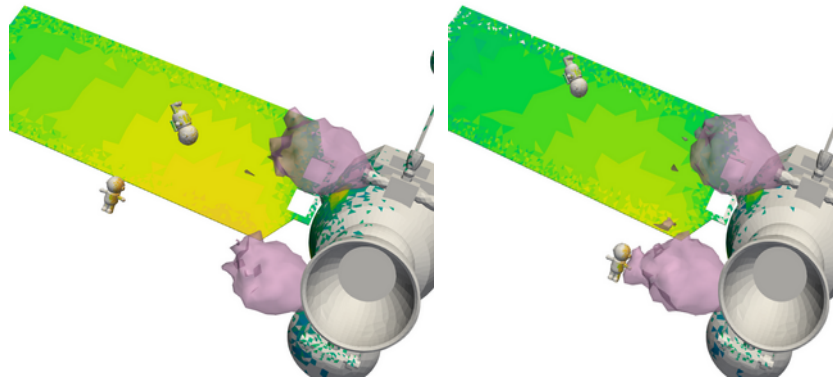


Figure 32. Illustration of a dynamic translation of surfaces

#### IV.d.2) Plume

The **plume** folder illustrates the use of source\_plume to load analytical plume profile per model of M. Woronowicz. Below we compare the plume profiles and surface incident momentum flux for a heavier VCM and a lighter helium population.

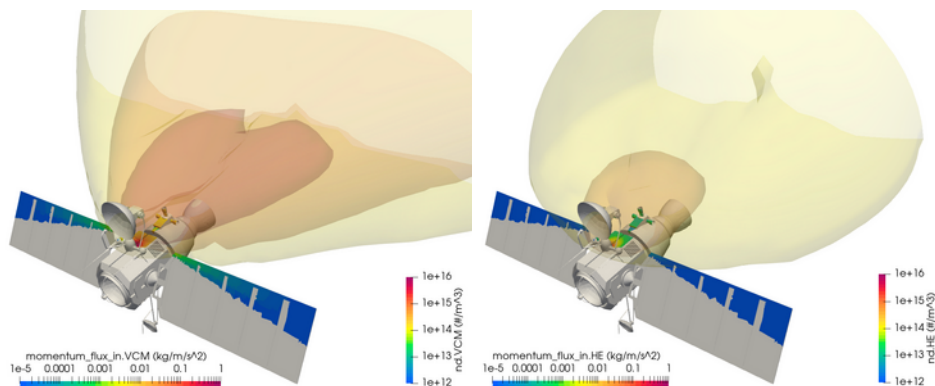


Figure 33. Analytical plume model for a heavier VCM (left) and lighter helium (right) population

## V. References

---

- [1] L. Brieda, "Numerical Model for Molecular and Particulate Contamination Transport," *Journal of Spacecraft and Rockets*, Vol. 56, No. 2, 2019
- [2] C. Birdsall and A. Langdon, *Plasma physics via Computer Simulations*, Institute of Physics Publishing, 2000.
- [3] G. Bird, *Molecular Gas Dynamics and the Direct Simulation of Gas Flows*, Oxford Science Publications, 1994.
- [4] H. Shin, Y. Lee and J. Jurng, "Spherical-shaped ice particle production of spraying water in a vacuum chamber," *Applied Thermal ENGINEERING*, pp. 439-454, 2000.
- [5] M. S. Woronowicz, "Highlights of Transient Plume Impingement Model Validation and Applications," in *42nd AIAA Thermophysics Conference*, 2011.
- [6] J. Koo, *Hybrid PIC-MCC computational modeling of Hall Thrusters*, Aerospace Engineering and Scientific Computing, University of Michigan, 2005.
- [7] A. Tribble, *Fundamentals of Contamination Control*, SPIE, 2000.
- [8] ASTM International, "Standard Test Method for Contamination Outgassing Characteristics of Spacecraft Materials (ASTM-E1559)," 2009.
- [9] W. Fang, M. Shillor, E. Stahel, E. Epstein, C. Ly, M. J. and E. Zaron, "A Mathematical Model for Outgassing And Contamination," *SIAM Journal of Applied Math*, vol. 51, no. 5, 1991.
- [10] A. C. Tribble, B. Boyadjian, J. Davis, J. Haffner and E. and McCullough, "Contamination control engineering design guidelines," NASA Contractor Report 4740, 1996.
- [11] IEST, "Product Cleanliness Levels Applications, Requirements, and Determinations (IEST-STD-CC1246D)," 2002.
- [12] A. Klavins and A. L. Lee, "Spacecraft particulate contaminant redistribution," *Optical system contamination effects, measurement, control*, vol. 777, pp. 236-244, 1987.
- [13] R. Perry, "A Numerical Evaluation of the Correlation of Surface Cleanliness Level and Percent Area Coverage," in *SPIE Optics and Photonics*, 2006.
- [14] F. White, *Viscous Fluid Flow*, New York: McGraw-Hill, 1991.